

# FIRE SEVERITY AND FIRE RESISTANCE IN STRUCTURAL FIRE ENGINEERING (SFE) DESIGN

Ruben Van Coile

- I. Introduction – Severity vs resistance
- II. Structures and fire – The facts
- III. What we want to achieve – The goals
- IV. The how – Fire engineering approach
- V. Opportunities of SFE (and risks)
  - a) Lane substitutions
  - b) Clarifying fire severity
  - c) More safety, lower cost
  - d) More safety, lower lifetime cost
  - e) Designing for performance





# Introduction

*Resistance vs. Severity*



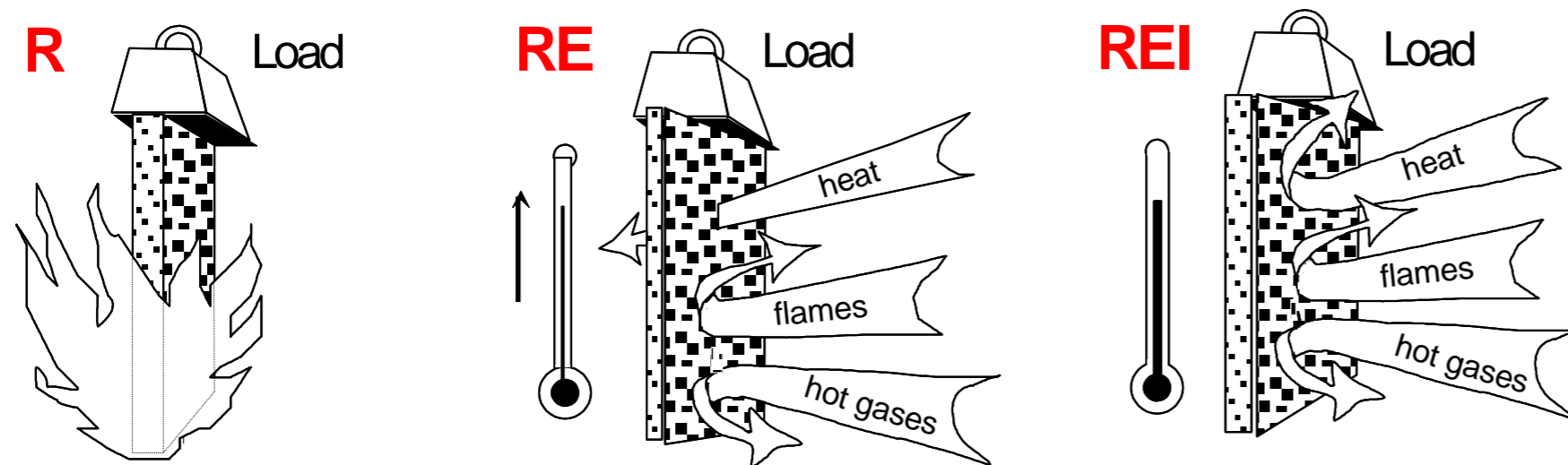


# FIRE SEVERITY VS RESISTANCE

The standard framework

Design requirement  $r \geq e$

Resistance  
(ability to resist fire)



Why?

Scientific characterization for safety

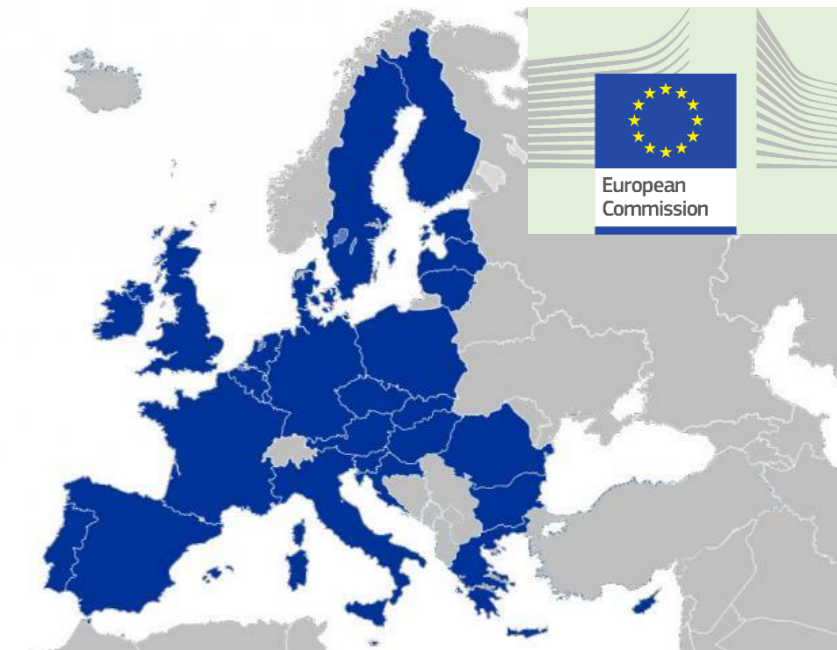
Historic reasons

Construction Products Regulation

Single market

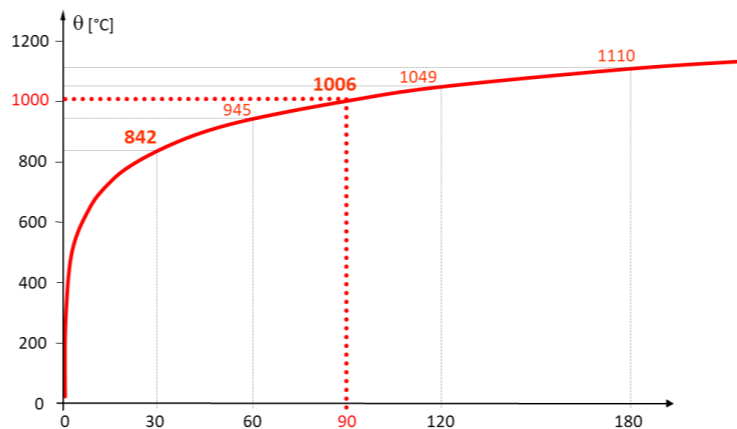
- Free circulation of goods
- Common terminology

[http://ec.europa.eu/growth/sectors/construction/product-regulation\\_en](http://ec.europa.eu/growth/sectors/construction/product-regulation_en)



www.secowarwick.com

Villa Real, P. (2012). COST Action TU0904 Malta.



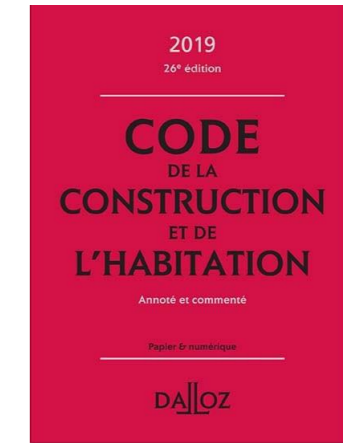
# FIRE SEVERITY VS RESISTANCE

The standard framework

Occupancy type; Building height; Sprinklers

Design requirement  $r \geq e$   
 Fire severity

Above 130m



**Table A2 Minimum periods of fire resistance**

Purpose group of building	Minimum periods of fire resistance (minutes) in a:					
	Basement storey <sup>(R)</sup> including floor over		Ground or upper storey			
	Depth (m) of a lowest basement		Height (m) of top floor above ground, in a building or separated part of a building			
	More than 10	Not more than 10	Not more than 5	Not more than 18	Not more than 30	More than 30
<b>1. Residential:</b>						
a. Block of flats						
– not sprinklered	90	60	30*	60**†	90**	Not permitted
– sprinklered	90	60	30*	60**†	90**	120**
b. Institutional	90	60	30*	60	90	120#
c. Other residential	90	60	30*	60	90	120#
<b>2. Office:</b>						
– not sprinklered	90	60	30*	60	90	Not permitted
– sprinklered <sup>(2)</sup>	60	60	30*	30*	60	120#
<b>3. Shop and commercial:</b>						
– not sprinklered	90	60	60	60	90	Not permitted
– sprinklered <sup>(2)</sup>	60	60	30*	60	60	120#
<b>4. Assembly and recreation:</b>						
– not sprinklered	90	60	60	60	90	Not permitted
– sprinklered <sup>(2)</sup>	60	60	30*	60	60	120#
<b>5. Industrial:</b>						
– not sprinklered	120	90	60	90		
– sprinklered <sup>(2)</sup>	90	60	30*	60		
<b>6. Storage and other non-residential:</b>						
a. any building or part not described elsewhere:						
– not sprinklered	120	90	60	90		
– sprinklered <sup>(2)</sup>	90	60	30*	60		
b. car park for light vehicles:						
i. open sided car park <sup>(3)</sup>	Not applicable	Not applicable	15*+	15*+ <sup>(4)</sup>		
ii. any other car park	90	60	30*	60		



Table 7.2.1.1 Fire Resistance Ratings for Type I Through Type V Construction (hr)

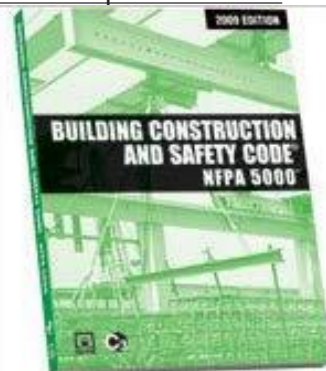
Construction Element	Type I		Type II			Type III		Type IV	Type V	
	442	332	222	111	000	211	200	2HH	111	000
<b>Exterior Bearing Walls<sup>a</sup></b>										
Supporting more than one floor, columns, or other bearing walls	4	3	2	1	0 <sup>b</sup>	2	2	2	1	0 <sup>b</sup>
Supporting one floor only	4	3	2	1	0 <sup>b</sup>	2	2	2	1	0 <sup>b</sup>
Supporting a roof only	4	3	1	1	0 <sup>b</sup>	2	2	2	1	0 <sup>b</sup>
<b>Interior Bearing Walls</b>										
Supporting more than one floor, columns, or other bearing walls	4	3	2	1	0	1	0	2	1	0
Supporting one floor only	3	2	2	1	0	1	0	1	1	0
Supporting roofs only	3	2	1	1	0	1	0	1	1	0
<b>Columns</b>										
Supporting more than one floor, columns, or other bearing walls	4	3	2	1	0	1	0	H	1	0
Supporting one floor only	3	2	2	1	0	1	0	H	1	0
Supporting roofs only	3	2	1	1	0	1	0	H	1	0
<b>Beams, Girders, Trusses, and Arches</b>										
Supporting more than one floor, columns, or other bearing walls	4	3	2	1	0	1	0	H	1	0
Supporting one floor only	2	2	2	1	0	1	0	H	1	0
Supporting roofs only	2	2	1	1	0	1	0	H	1	0
<b>Floor/Ceiling Assemblies</b>	2	2	2	1	0	1	0			
<b>Roof/Ceiling Assemblies</b>	2	1½	1	1	0	1	0			
<b>Interior Nonbearing Walls</b>	0	0	0	0	0	0	0			
<b>Exterior Nonbearing Walls<sup>c</sup></b>	0 <sup>b</sup>	0 <sup>b</sup>	0 <sup>b</sup>	0 <sup>b</sup>	0 <sup>b</sup>	0 <sup>b</sup>	0 <sup>b</sup>			

H: Heavy timber members (see text for requirements).

<sup>a</sup>See 7.3.2.1.

<sup>b</sup>See Section 7.3.

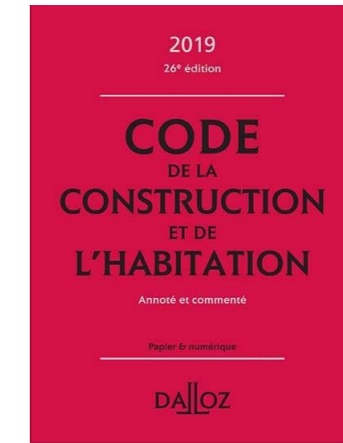
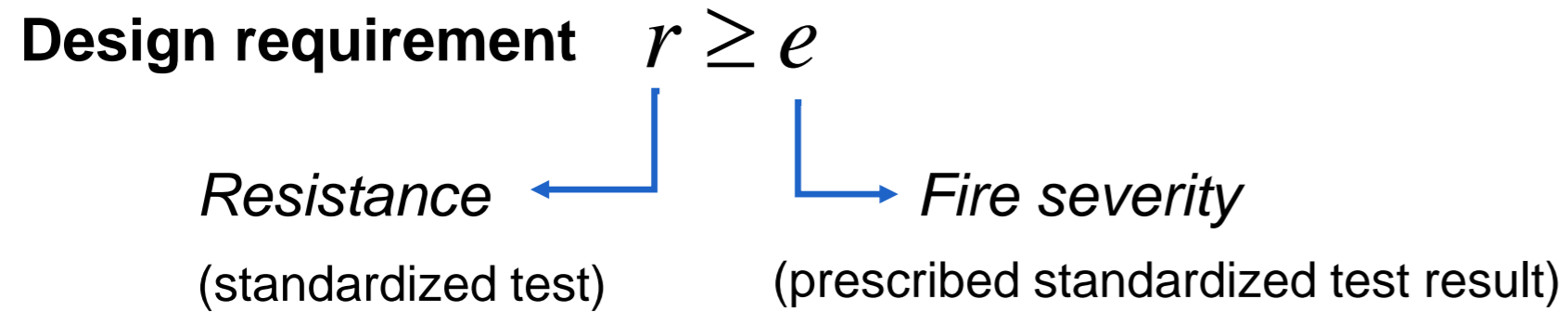
<sup>c</sup>See 7.2.3.2.12, 7.2.4.2.3, and 7.2.5.6.8.





# FIRE SEVERITY VS RESISTANCE

*The standard framework*



## The mechanism at work

*How is safety achieved?*



Innovation fire, 22/05/1967, Brussels



## In a standard (prescriptive) framework

***progress relies on lessons learned from failure.***



*Prof. D. Drysdale*

Spinardi, et al. (2017). *Fire technology*, 53(3), 1011-1037.



# IS THIS REASONABLE ?

*Fire resistance and severity, standard framework*



Relative level of complexity	(1) Simple
Design solutions	Prescriptive guidelines
Fire safety job	Code consultancy



urbanlink.be

the-shard.com

dailymail.co.uk



*For non-common buildings: **adopt a fire engineering approach***



# WHAT IS FIRE ENGINEERING ?

## Institution of Fire Engineers

**Fire engineering** is the **application of scientific and engineering principles, rules (codes), and expert judgement, based on an understanding of the phenomena and effects of fire and of the reaction and behavior of people to fire, to protect people, property and the environment from the destructive effects of fire**



# IMPLICATION FOR FIRE RESISTANCE?

*Understanding of the phenomena*

*To protect people, property and the environment*

*Apply scientific and engineering principles*

II. Structures and fire – The facts

III. What we want to achieve – The goals

IV. The how – Fire engineering approach



# Structures & fire

*“understanding of  
the phenomena”*





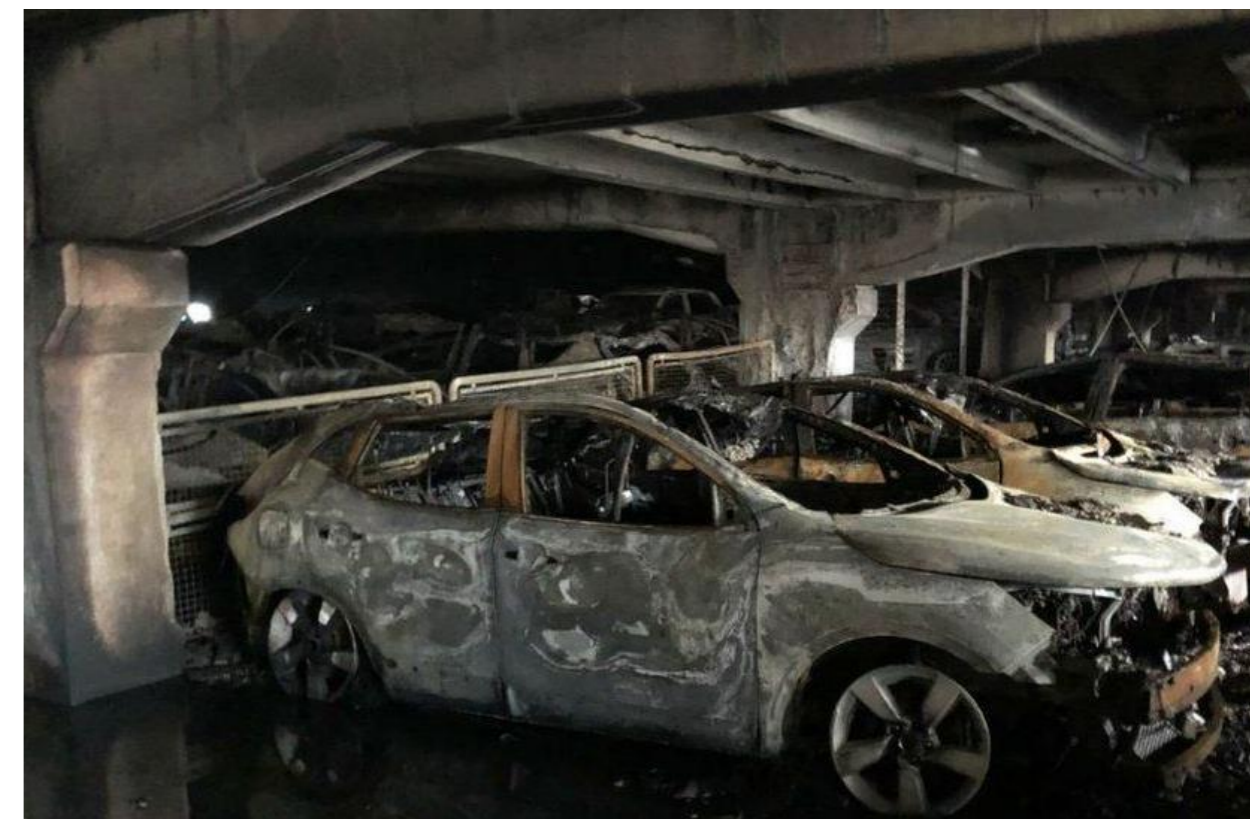
# FIRE EXPOSURE

## Complex phenomenon

- Ventilation
- Fire load (type; position)
- Compartment (size; lining)
- Fire brigade intervention
- ...



Francois Malan. [www.flickr.com](http://www.flickr.com)



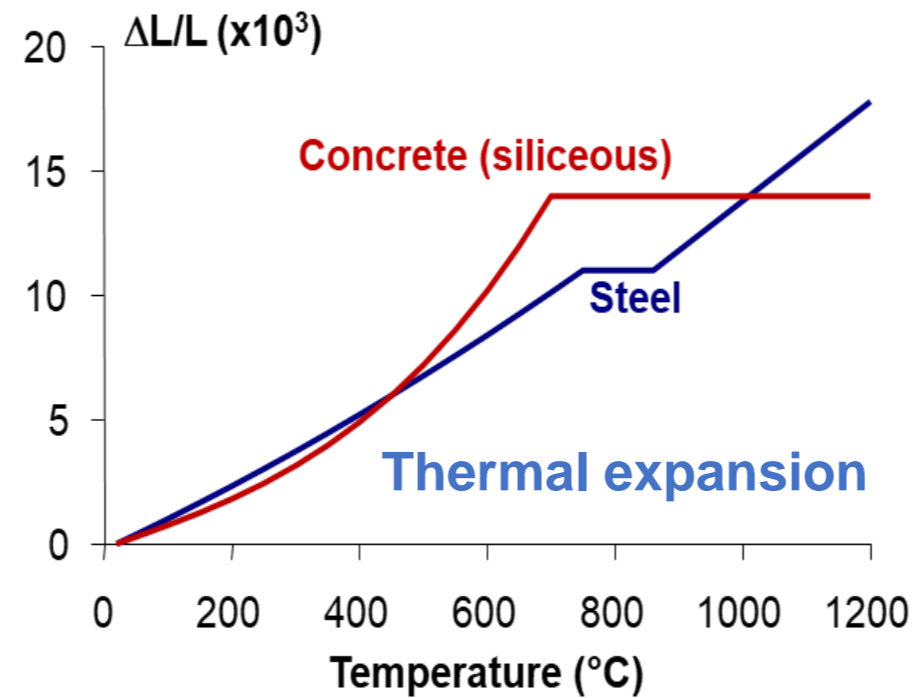
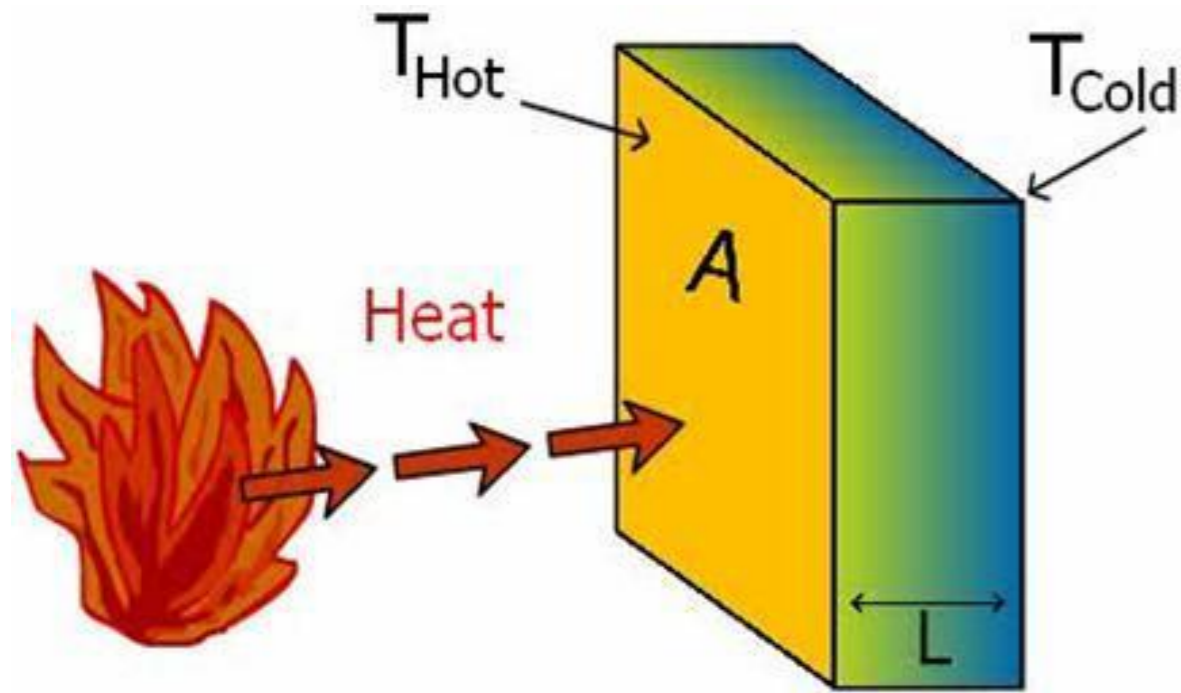
Merseyside Fire and Rescue; <https://www.bbc.com/news/uk-england-merseyside-42542556>



Beji et al. (2015). *Fire Safety Journal*, 76, 9-18.

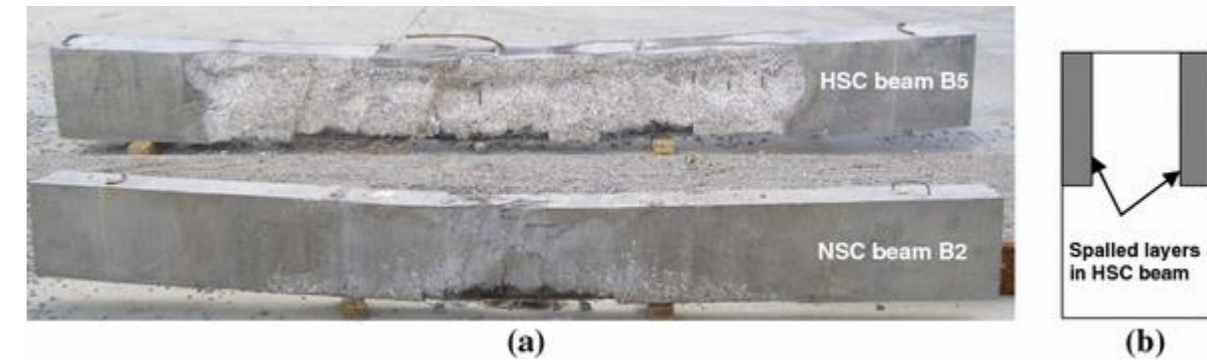


# RESPONSE – MATERIAL LEVEL



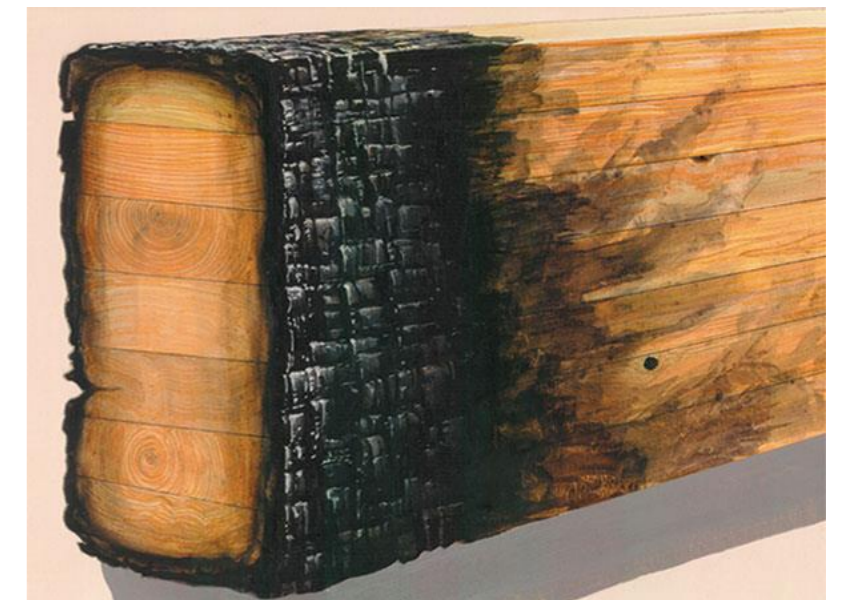
Gernay, T. (2018). Lecture notes Structural Fire Engineering.

## Concrete spalling



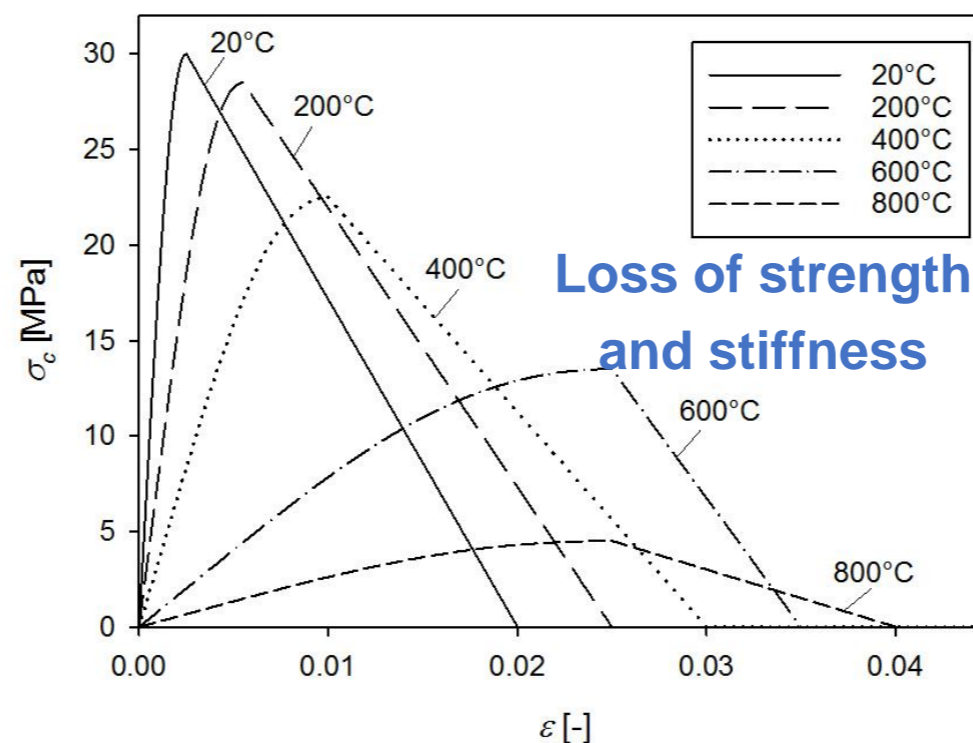
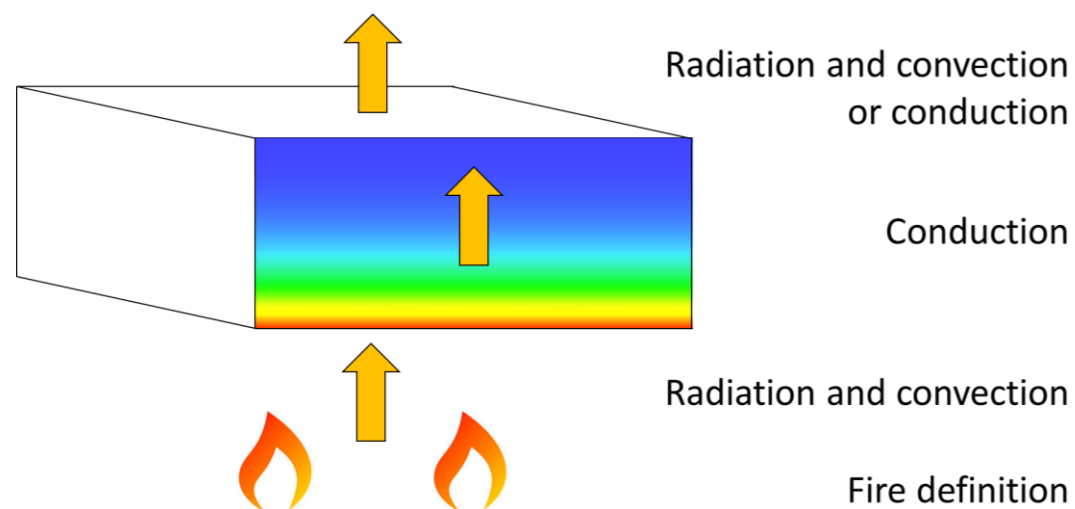
Dwaikat, M.B. & Kodur, V.K.R. Fire Technol (2010) 46: 251

## Timber charring



White & Woeste (2013). STRUCTURE magazine, November 2013, 38-40.

www.nist.gov



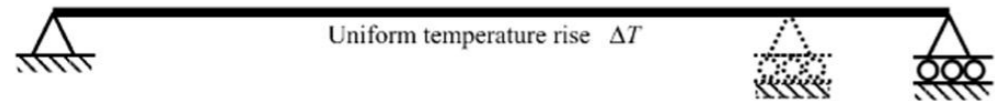


# RESPONSE – ELEMENT LEVEL

## Uniform temperature effects

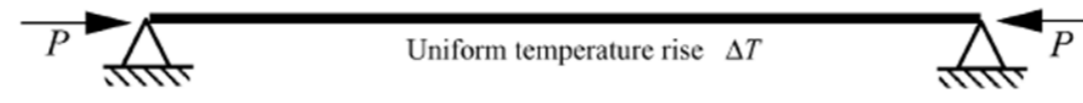
### Thermal expansion

uniform temperature increase  $\Delta T$ , averaged  $\alpha$



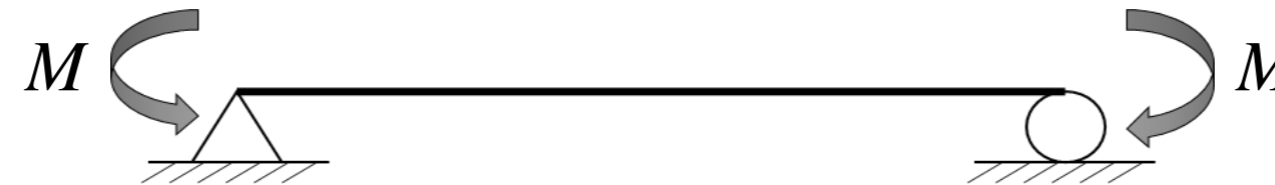
Usmani et al. (2001). *Fire Safety Journal*, 36(8), 721-744.

### Restrained



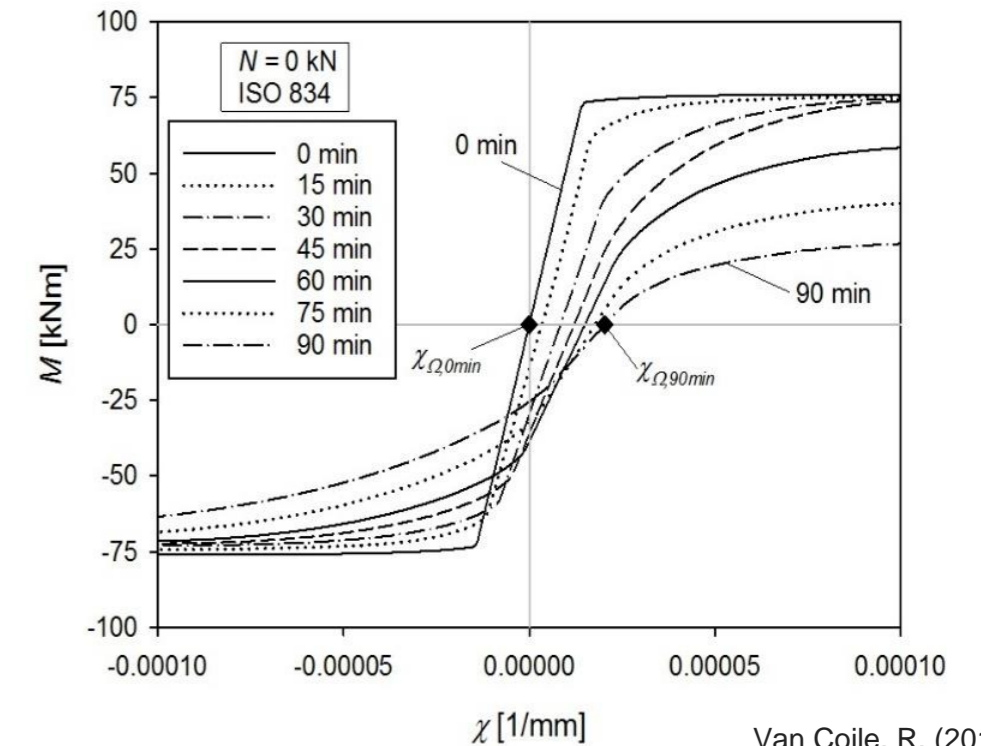
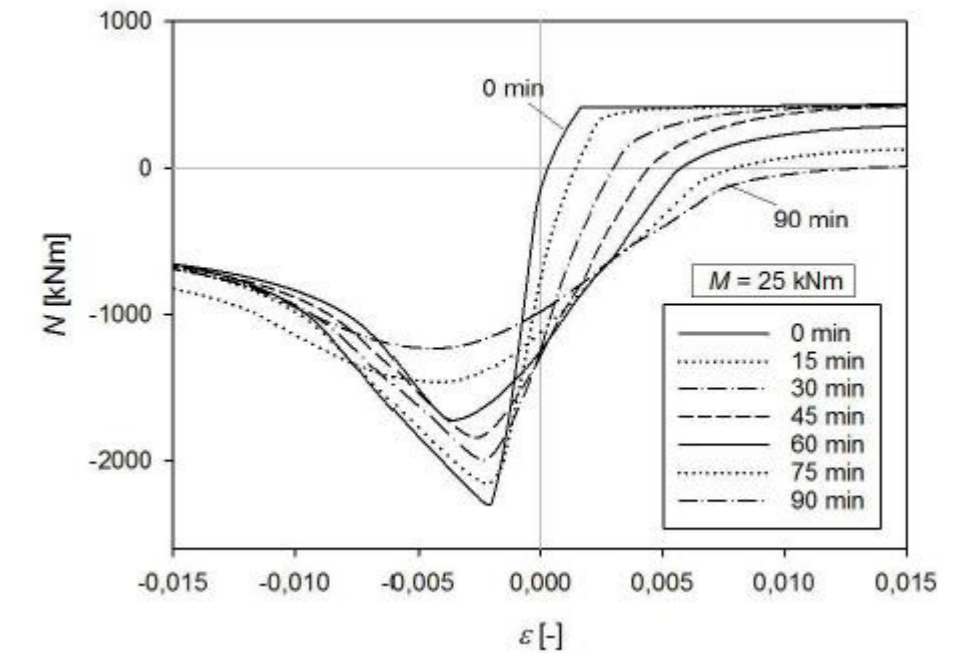
$$P = EA\varepsilon_m = -EA\varepsilon_T = -EA\alpha\Delta T$$

uniform temperature gradient  $\Delta T^*$ , averaged  $\alpha$



$$M = EI\chi_{th} = EI\alpha\Delta T^*$$

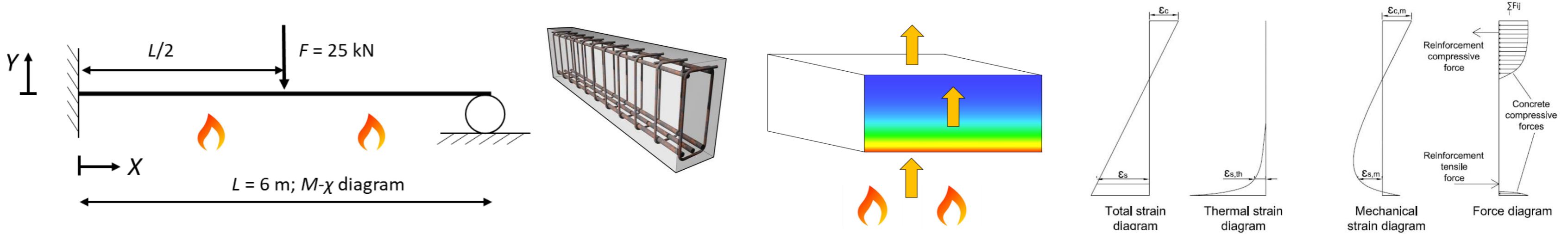
## Non-uniform temperature effects



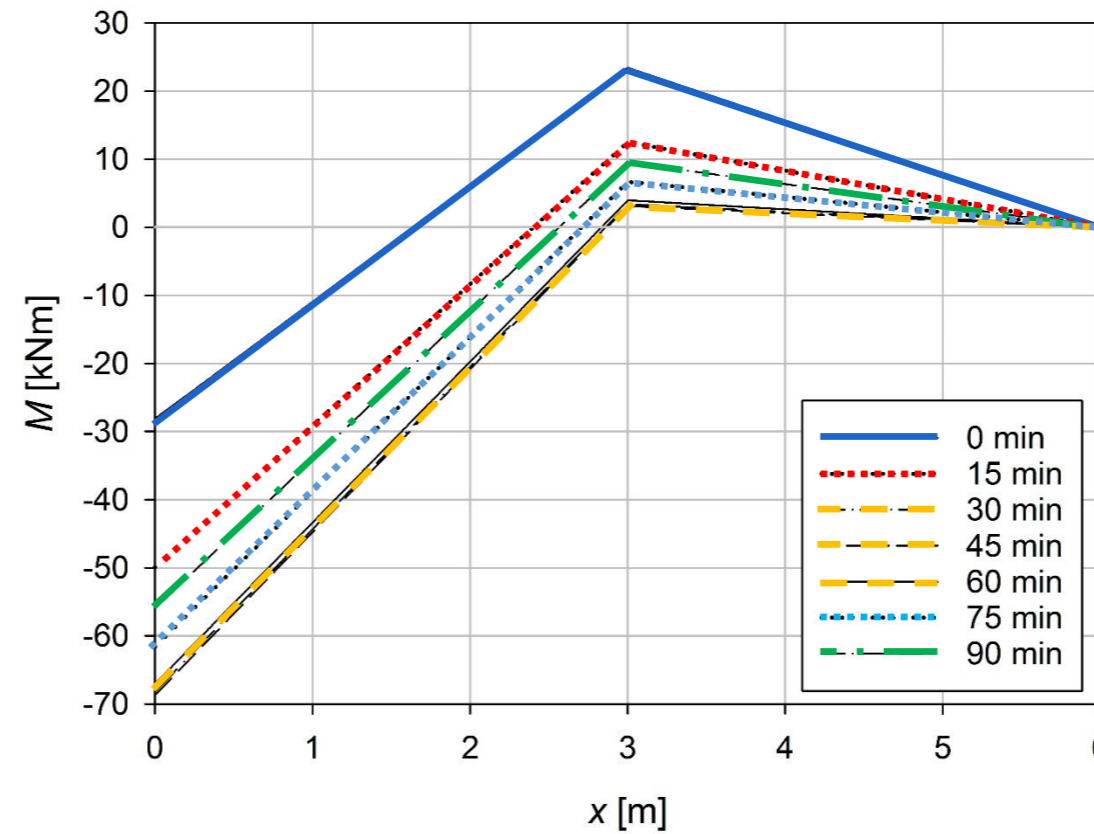
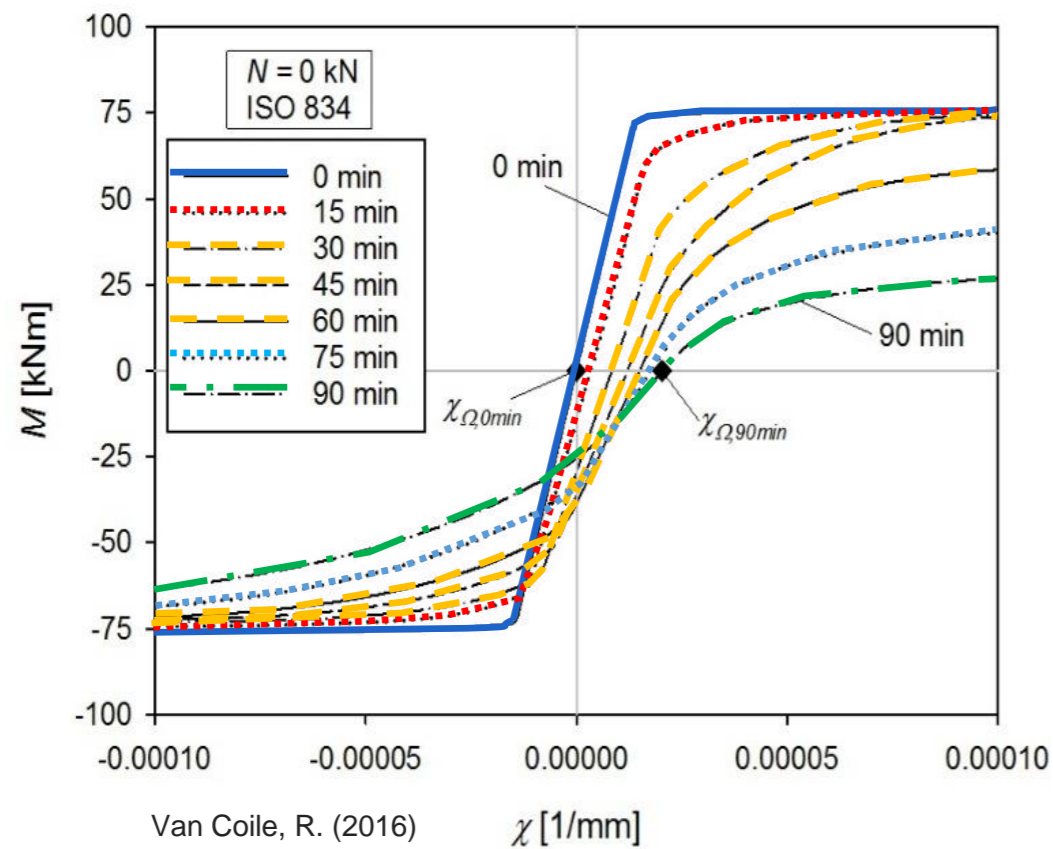
Van Coile, R. (2016)



# RESPONSE – ELEMENT LEVEL – EXAMPLE



Internal restraint / compatibility





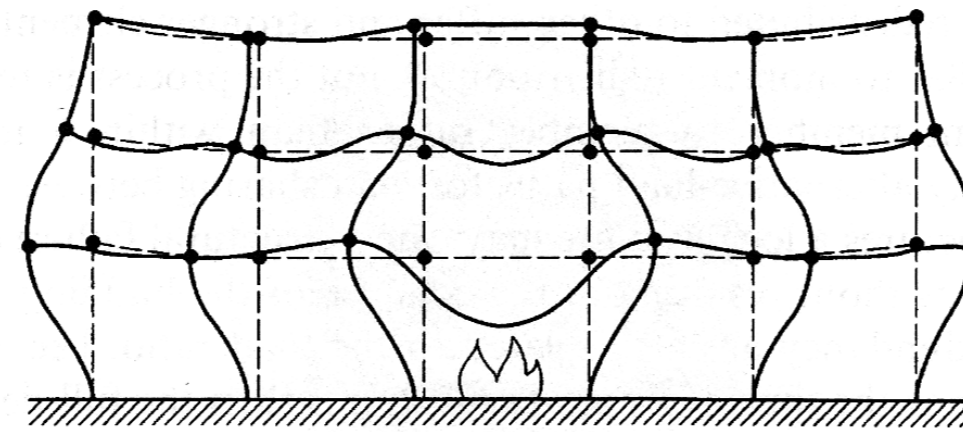
# RESPONSE – SYSTEM LEVEL & COOLING

## Interaction with remainder of structure



Wikipedia. Broadgate fire.

### Positive effect

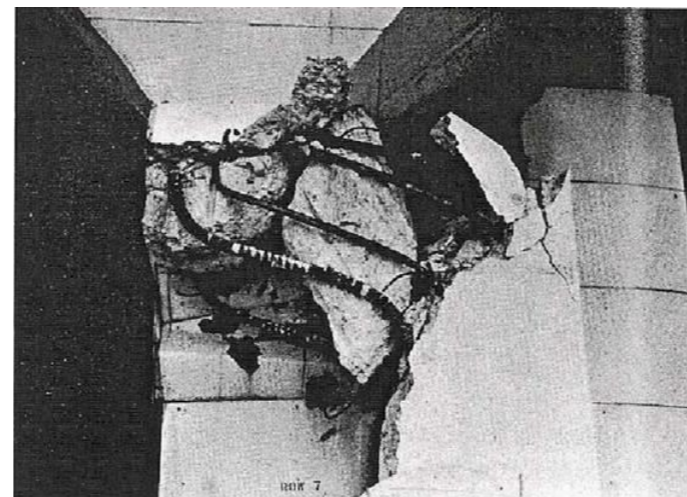


Buchanan and Abu (2017)

### Negative effect

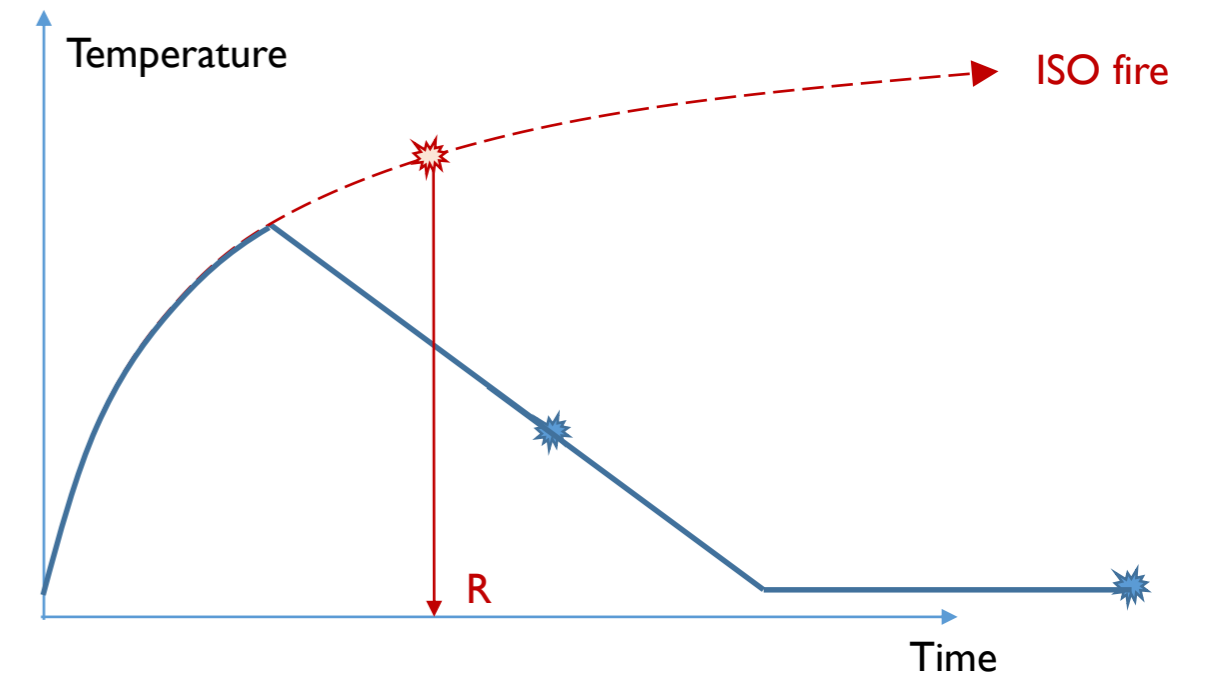


Gernay, T. (2018). Lecture notes Structural Fire Engineering.



## Cooling phase failures

- Thermal inertia (further heating)
- Strength loss in cooling
- Tension failure (permanent deformation)



Gernay, T. (2018). Lecture notes Structural Fire Engineering.

Gernay, T. (2019). Fire resistance and burnout resistance of reinforced concrete columns. *Fire Safety Journal*, 104, 67-78.



# CONSEQUENCES

“Iranian firefighters killed in collapse”



Agencia EFE

6 months reduced Chunnel service



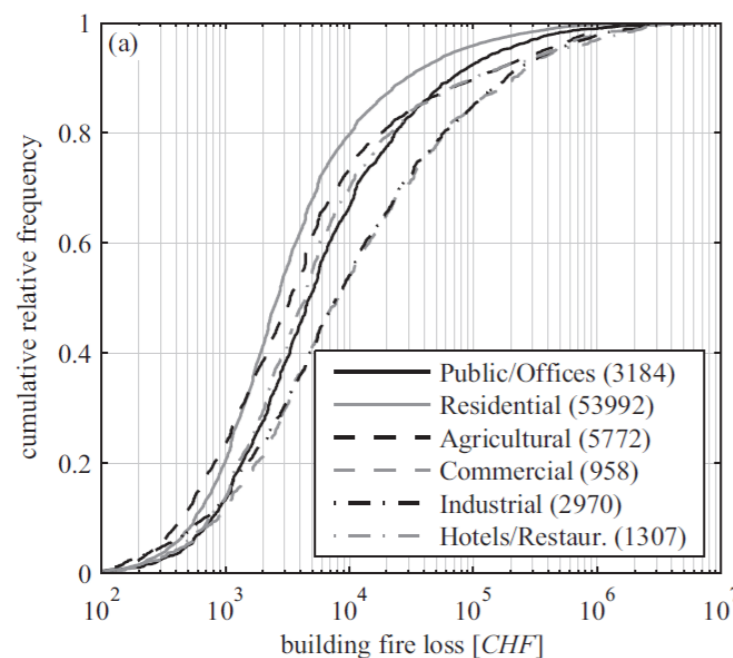
“Brazil museum fire: ‘incalculable loss’”



Globo.com

2000-2007  
Swiss insurance  
loss data

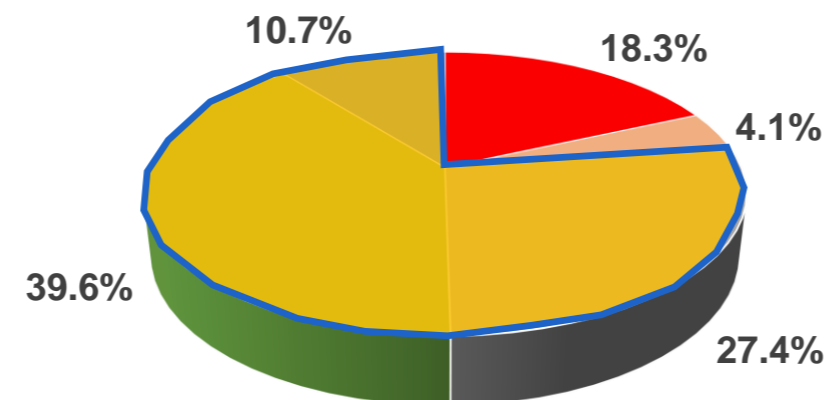
Fischer, K. (2014). Doctoral  
dissertation.



Economic “costs” of fire 2008-2010; 1% GDP

CTIF-World Fire Statistics Center 2016 n°21

**75% cost of fire result  
from prevention**



- Direct losses
- Indirect losses
- Cost of fire service
- Fire protection in buildings
- Fire insurance

“Sandoz chemical spill”

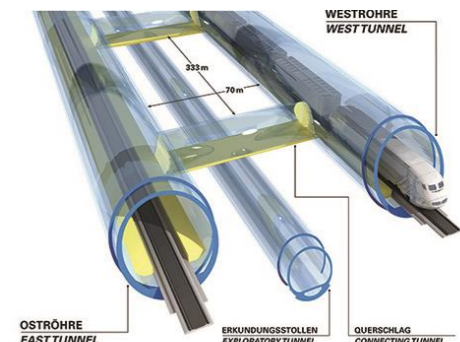




# Fire resistance

# goals

*“protect people,  
property and the  
environment”*





# GOALS FOR FIRE SAFETY

Particularly important for structural fire engineering



*SFPE Guide to Performance-based Fire Protection Engineering*

- **Life safety**
- **Property protection**
- **Environmental protection**
- **Continuity of operations**
- *Historic preservation*

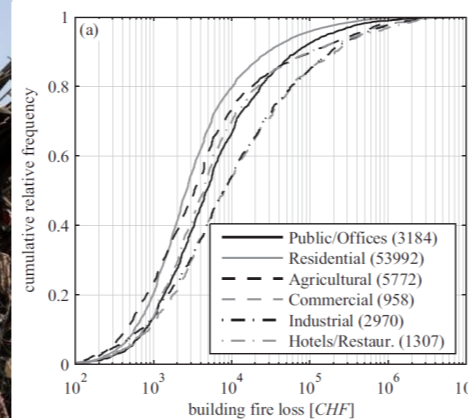
[There is an] *expectation that buildings will not collapse or allow fire to spread*

*Prof. L. Bisby*

Bisby, L. (2016). Lecture notes Structural Design for Fire

## Institution of Fire Engineers

*Fire engineering is the **application of scientific and engineering principles, rules (codes), and expert judgement, based on an understanding of the phenomena and effects of fire and of the reaction and behavior of people to fire, to **protect people, property and the environment** from the destructive effects of fire***





# GOALS FOR FIRE SAFETY

<i>Fire engineering sub-goals</i>	ISO 23932-1:2018	SFPE PBD Guide	Hadjisophocleous et al. (1998)	NFPA 5000 (2018)	BS 7974:2019
<b>Life safety (incl. fire fighters)</b>					X
<b>Property protection</b>				<i>'relates primary goals'</i>	X
<b>Continuity of operations</b>				<i>'incorporated in public welfare'</i>	<i>'operational resilience'</i>
<b>Environmental protection</b>				<i>'incorporated in public welfare'</i>	
<b>Historic preservation</b>				<i>'incorporated in public welfare'</i>	*
<b>Avoiding conflagration</b>					*
<b>Public welfare</b>			<i>'preventing public troubles'</i>		
<b>Cost-efficiency</b>					*

\* mentioned in text discussing *'fire functional objectives'*

**Over-arching Fire Engineering goal:** *Controlling fire risks to socio-economically acceptable levels, as part of the overall fire safety strategy*

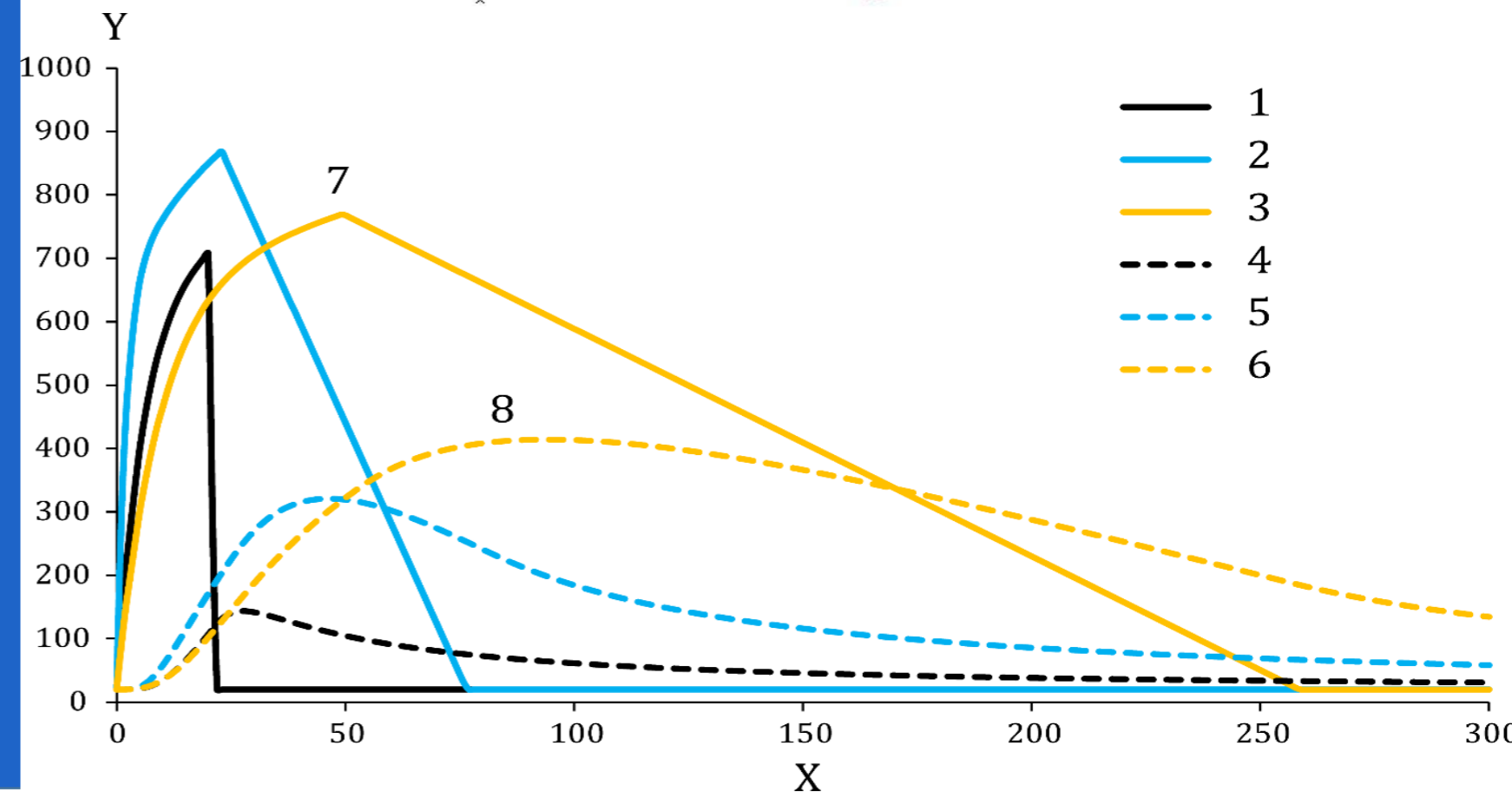
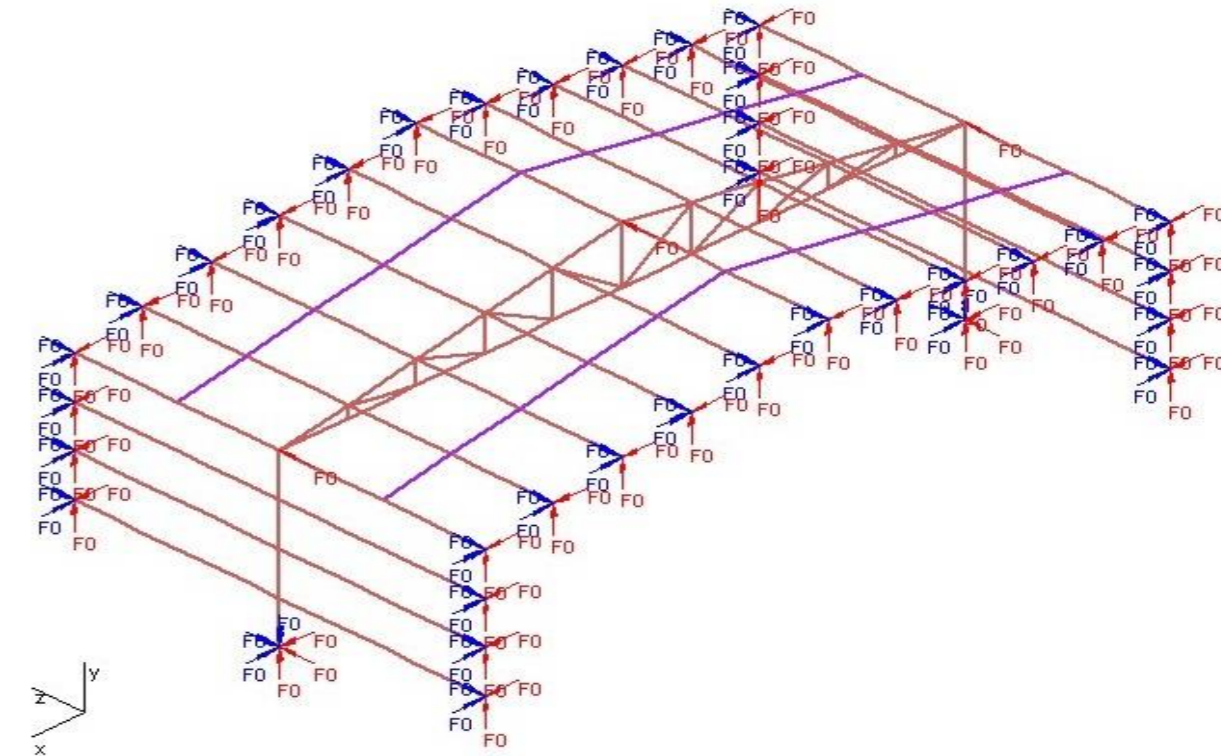
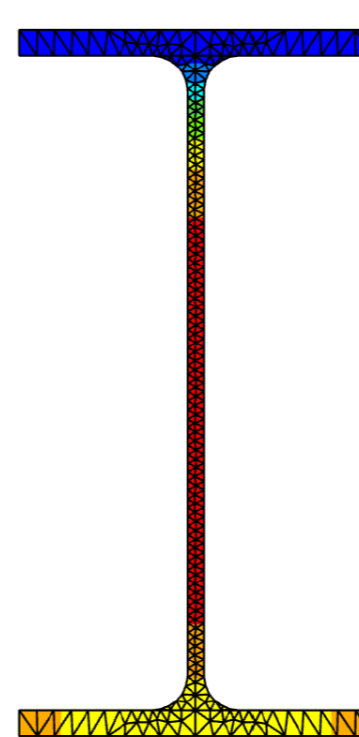


*Structural Fire Engineering objectives go beyond (indirect) code compliance*



# Fire engineering approach

“application of scientific and engineering principles”



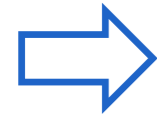
Gernay, T., Franssen, J.-M. (2018). SAFIR training. Johns Hopkins University (USA), Université de Liège (BE).

ISO TR 24679-6:2017. Fire safety engineering – Performance of structures in fire – Part 6: Example of an eight storey office concrete building. *International Organization for Standardization.*



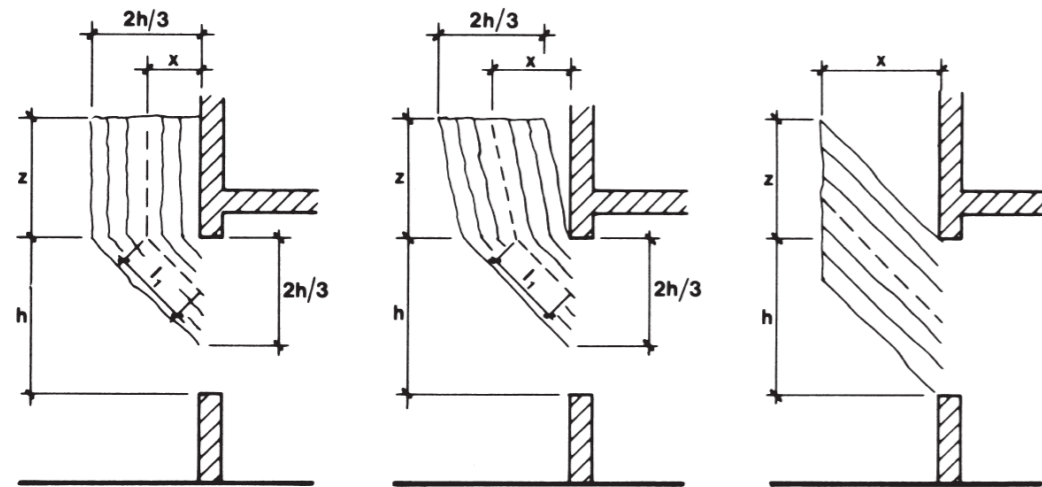
# CASE – LONDON HIGH-RISE SCULPTURE

Design beyond prescriptive guidance; SFE objective: no collapse



Evaluate background Eurocodes

Law, M. (1978). Fire safety of external building elements – the design approach. American Institute of Steel Construction Engineering Journal, 59-74



$$l_1 = \sqrt{x^2 + \left(\frac{h}{3}\right)^2} \triangleq \frac{h}{2}$$

$$X = z + l_1$$

Natural draught  
 $w > 0.8h$  wall above

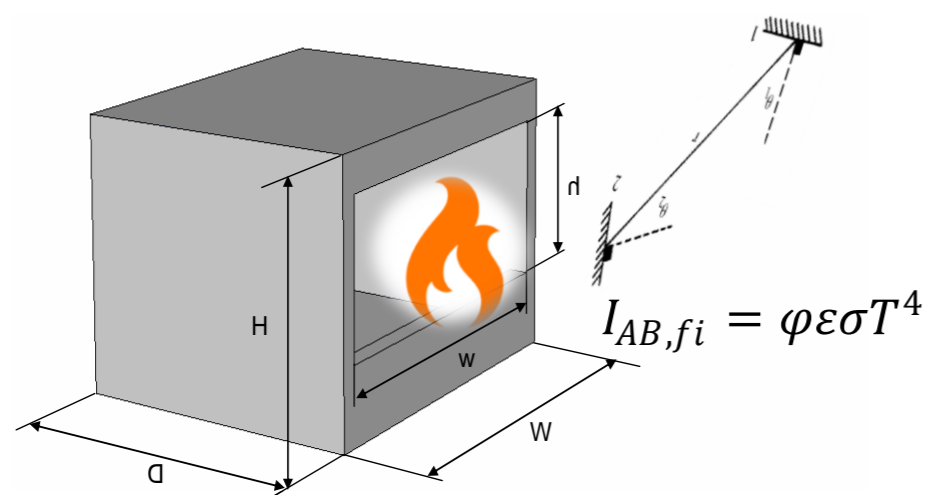
$$l_1 = \sqrt{x^2 + \left(\frac{h}{3}\right)^2}$$

$$X = \sqrt{z^2 + \left(x - \frac{h}{3}\right)^2} + l_1$$

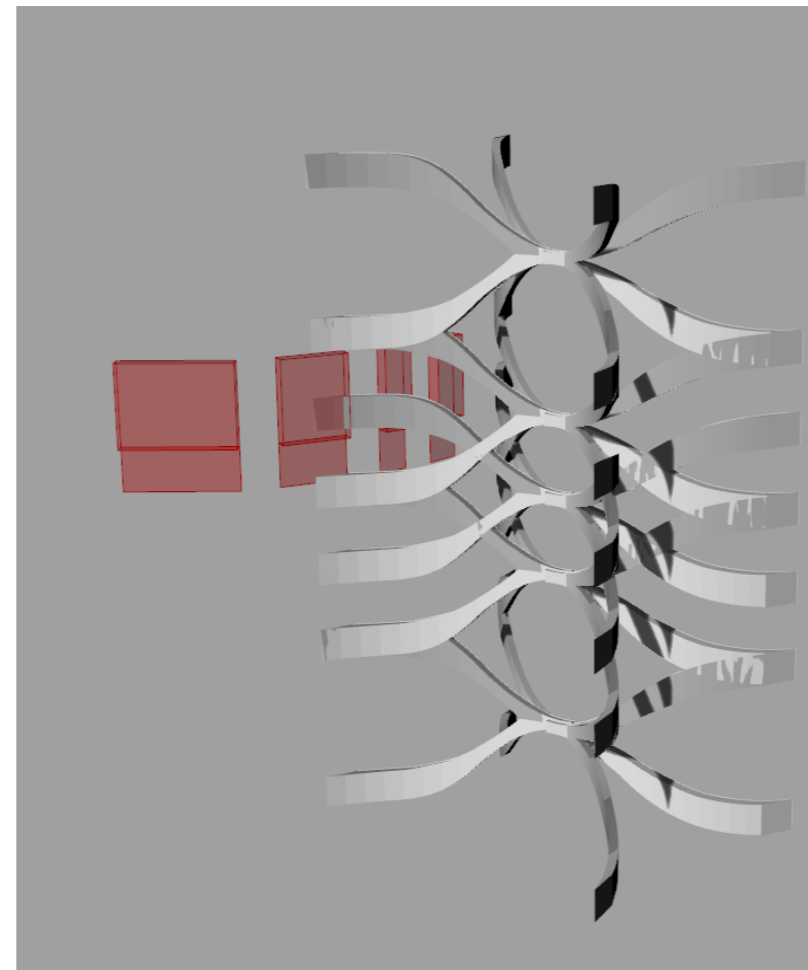
Natural draught  
 $w < 0.8h$  wall above  
or no wall above

$$X = \sqrt{z^2 + x^2}$$

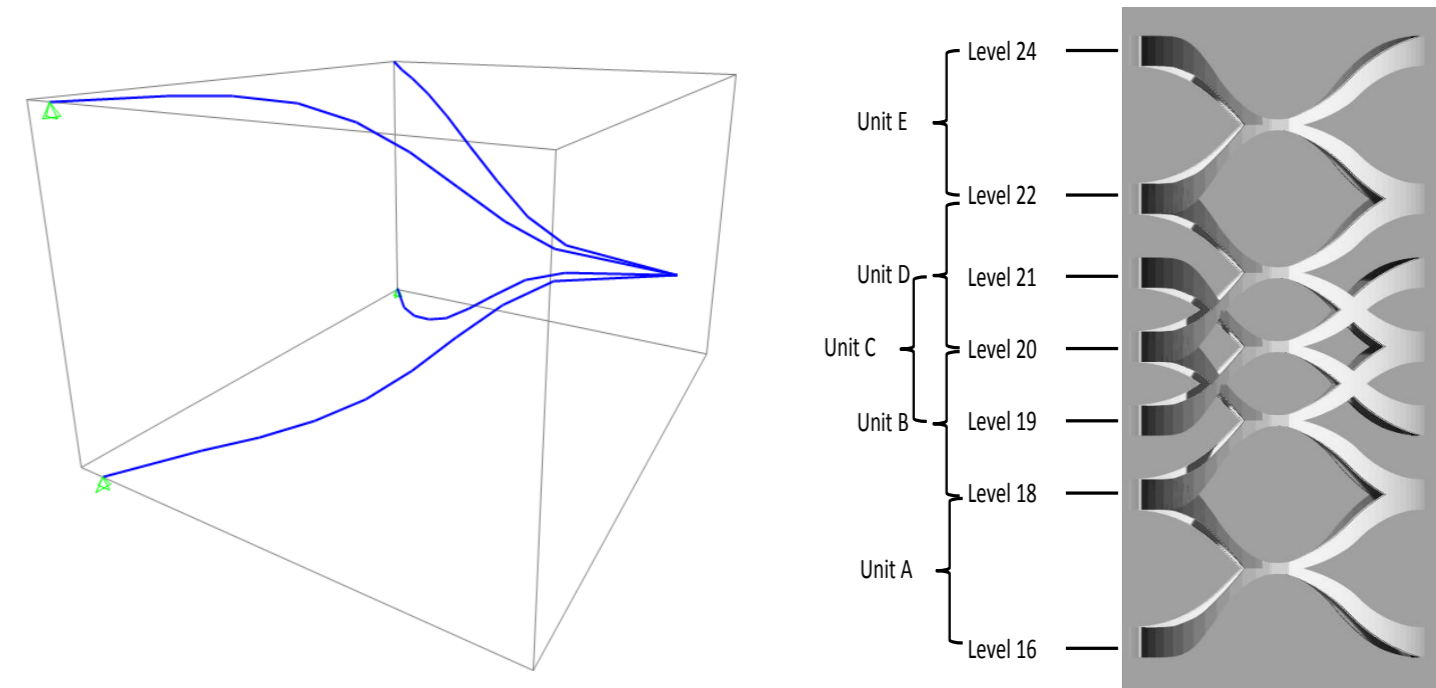
Forced draught  
wall or no wall above



$$I_{AB,fi} = \varphi \varepsilon \sigma T^4$$



Material at elevated temperature  
Load redistribution to other connections confirmed





# CASE – UNDERWATER TUNNEL PROTECTION

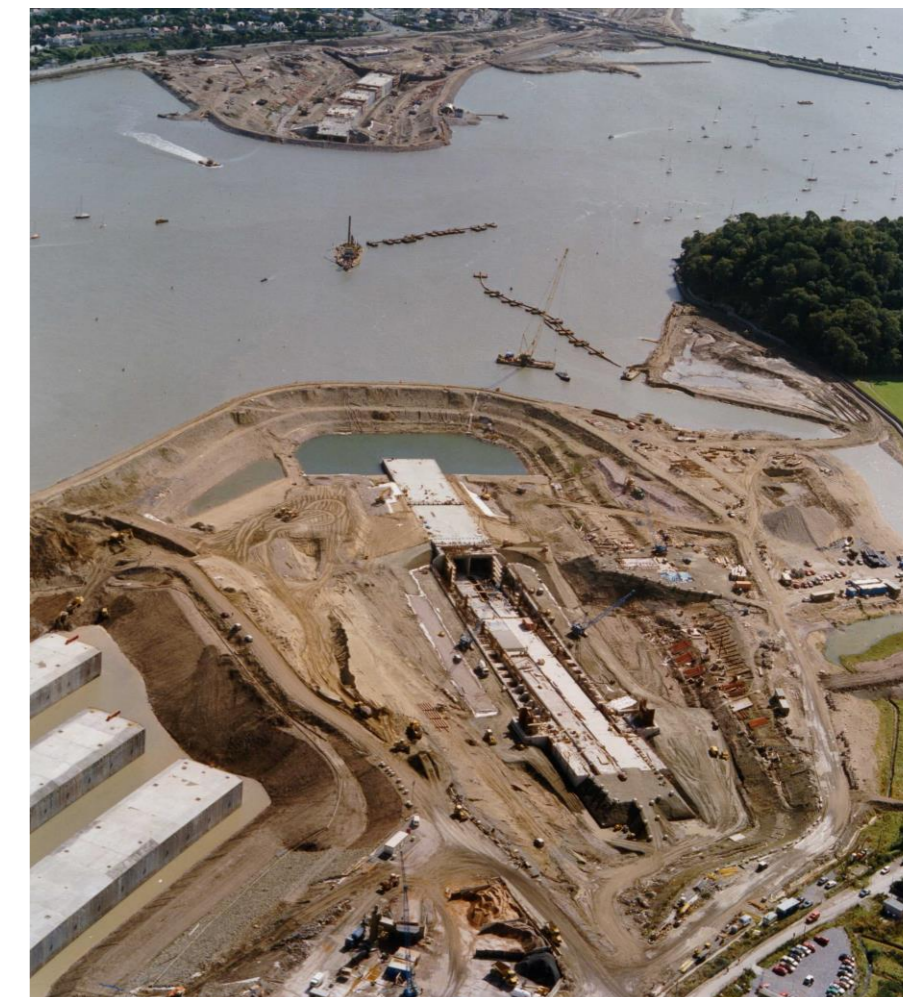
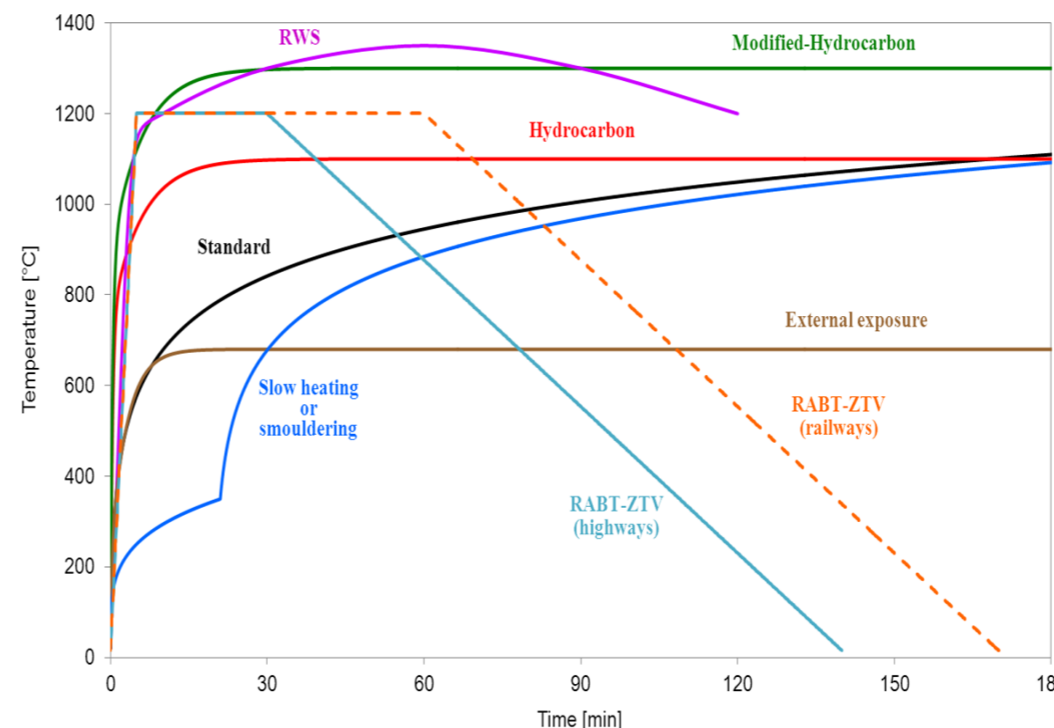
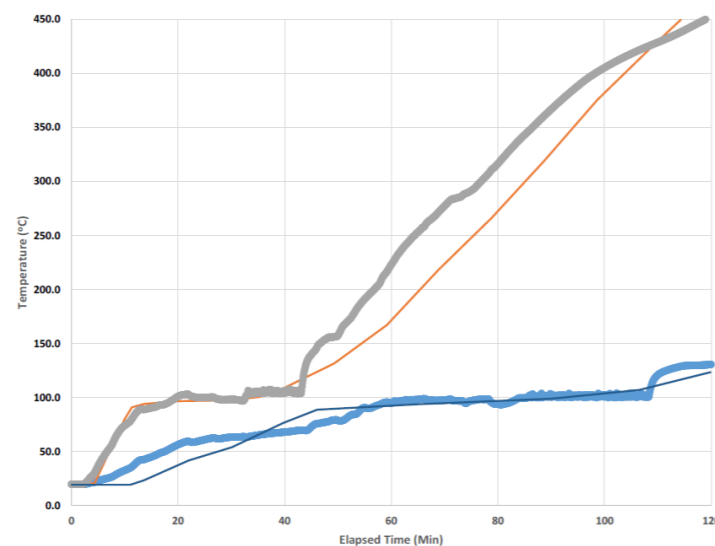
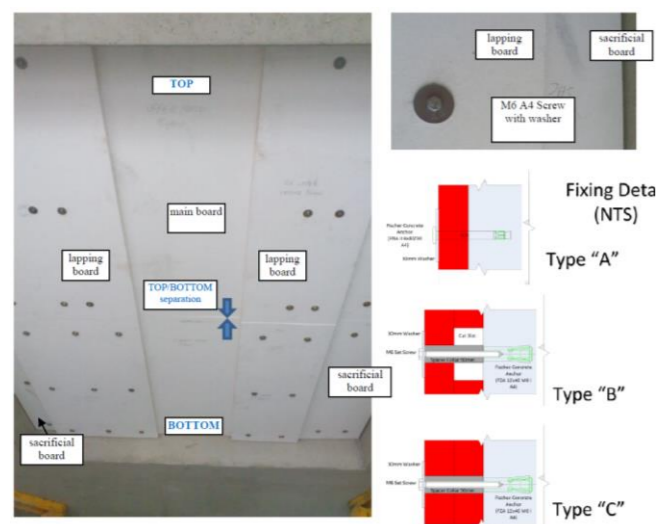
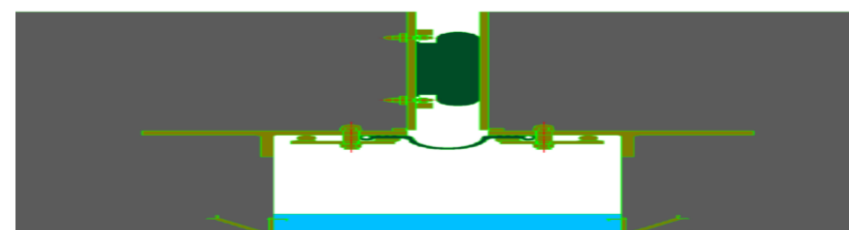
cases.ita-aites.org

Design beyond prescriptive guidance

SFE objective:

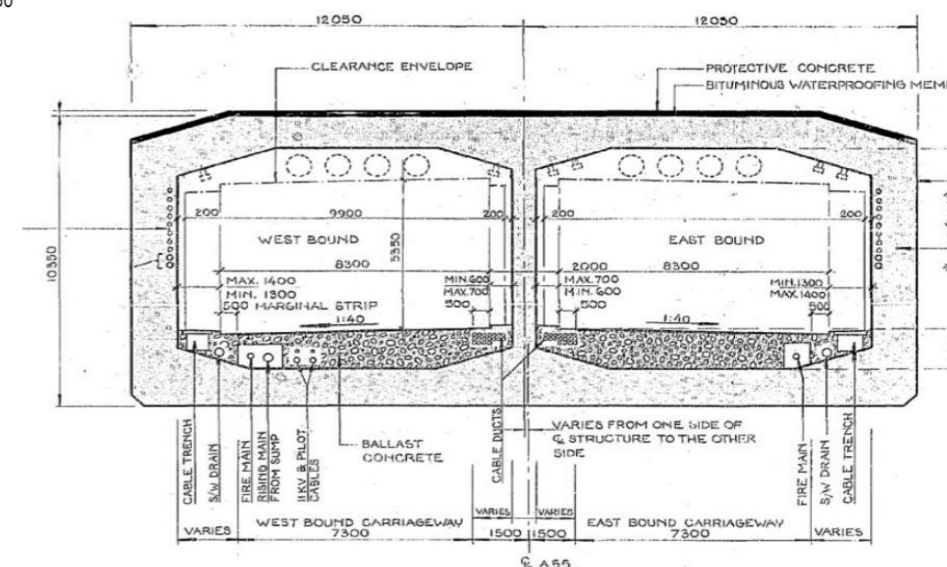
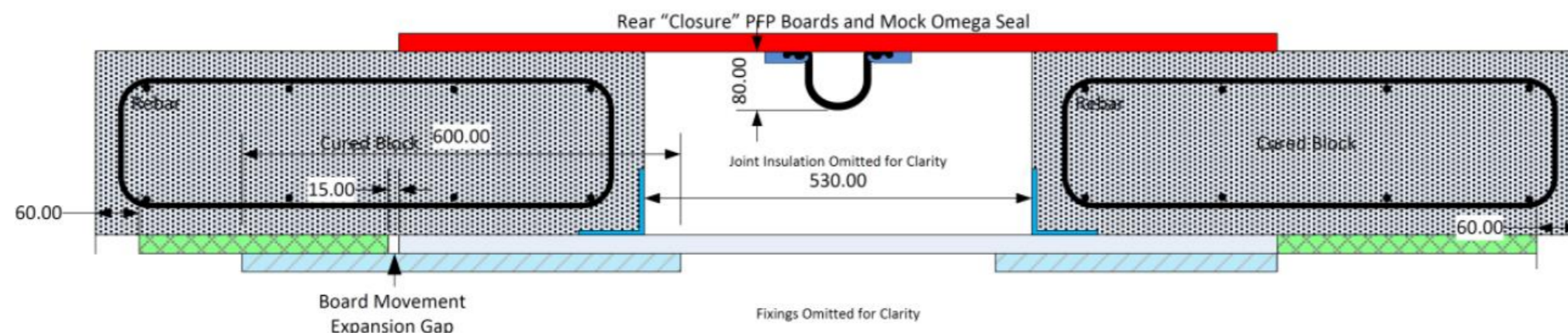
Omega seal < 120°C at 2 hours RWS

Element and dilatation joints vulnerable to fire



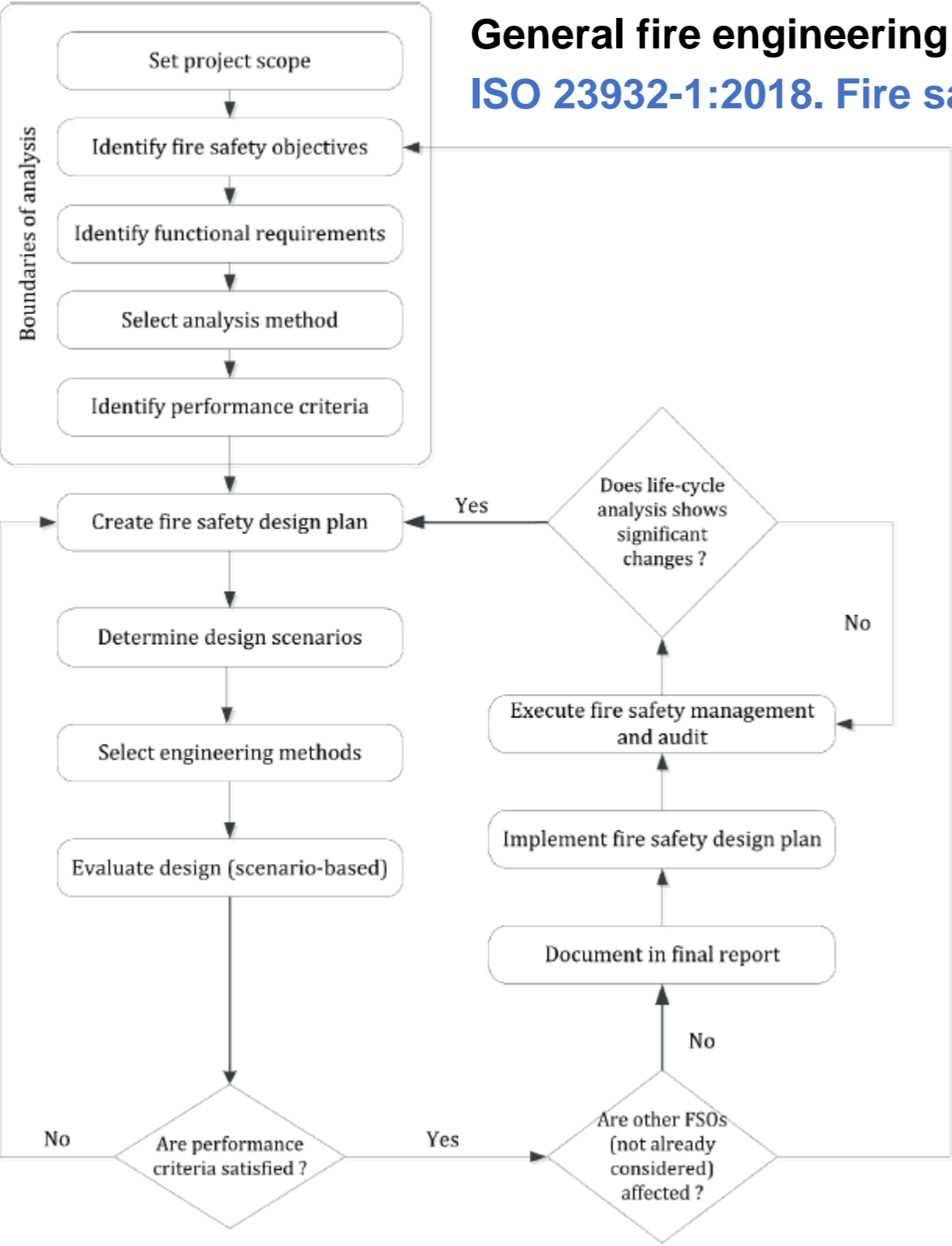
Tarada, F. (2018). Fire protection of tunnel joints for the A55 Conwy immersed tube tunnel. *International Symposium on Tunnel Safety and Security*, 14-16/03, Boras, Sweden.

Bisby, L. (2016). Lecture notes Structural Design for Fire





# STRUCTURAL FIRE ENGINEERING FRAMEWORK



**General fire engineering framework**

ISO 23932-1:2018. Fire safety engineering – General principles

*‘Normative’, not procedural*

**Structural fire engineering framework**

ISO 24679-1:2017. Fire safety engineering – Performance of structures in fire

- Step 1: Scope of the project (for fire safety of structures)
- Step 2: Identifying objectives, functional requirements and performance criteria
- Step 3: Trial design plan
- Step 4: Design fire scenarios and design fires
- Step 5: Thermal response of the structure
- Step 6: Mechanical response of the structure
- Step 7: Assessment against the fire safety objectives
- Step 8: Documentation of the design for fire safety of structures

**Introduce step-wise:**

**ISO TR 24679-6:2017**  
 Fire safety engineering –  
 Performance of structures in  
 fire – Part 6: Example of an  
 eight storey office concrete  
 building



# STRUCTURAL FIRE ENGINEERING FRAMEWORK

## Structural fire engineering framework

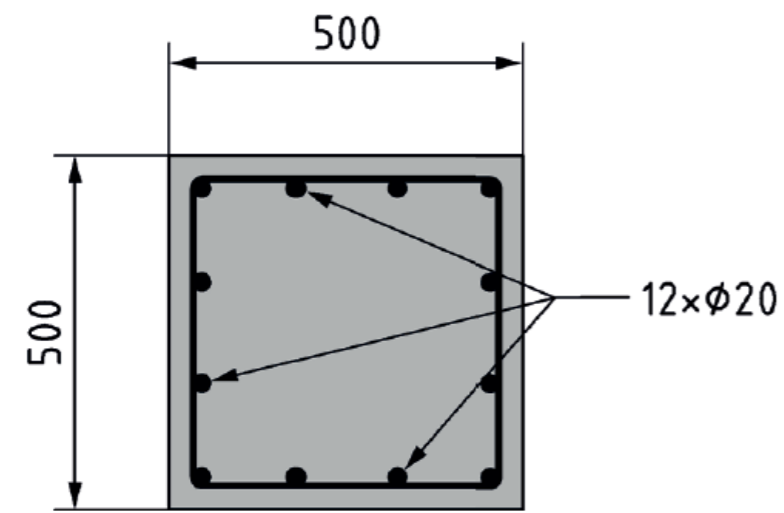
### ISO 24679-1:2017. Fire safety engineering – Performance of structures in fire

ISO TR 24679-6:2017. Fire safety engineering – Performance of structures in fire – Part 6:  
Example of an eight storey office concrete building. *International Organization for Standardization.*

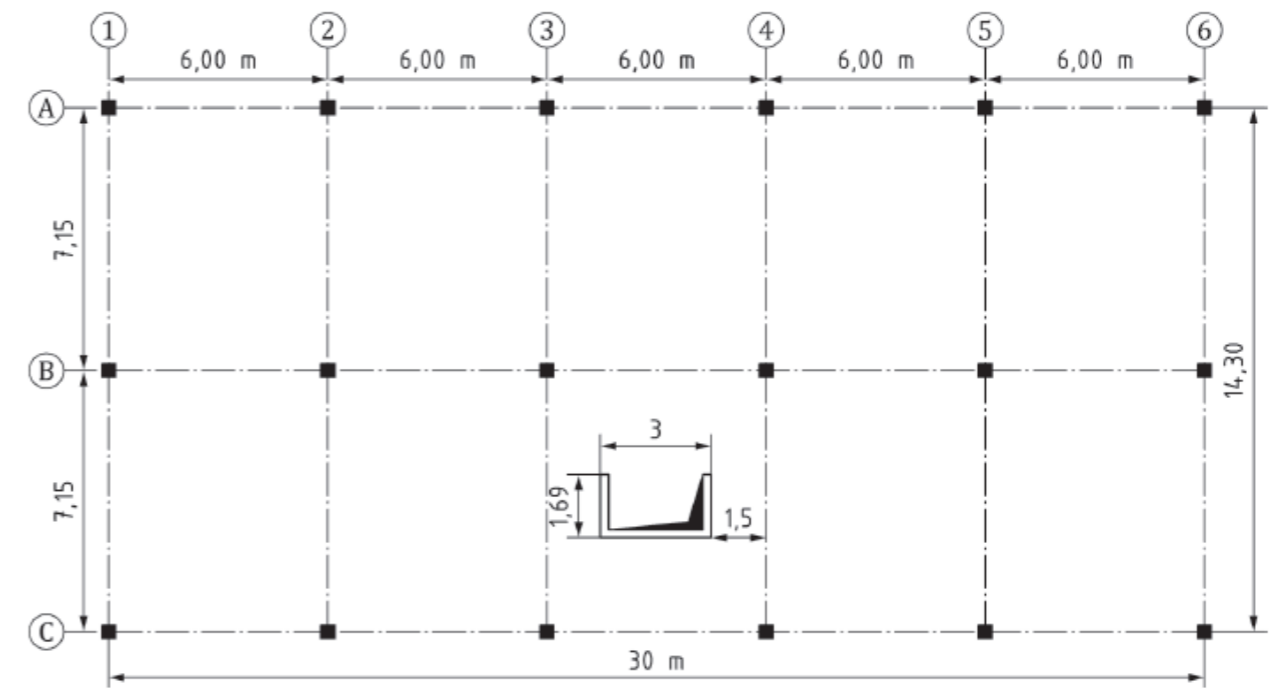
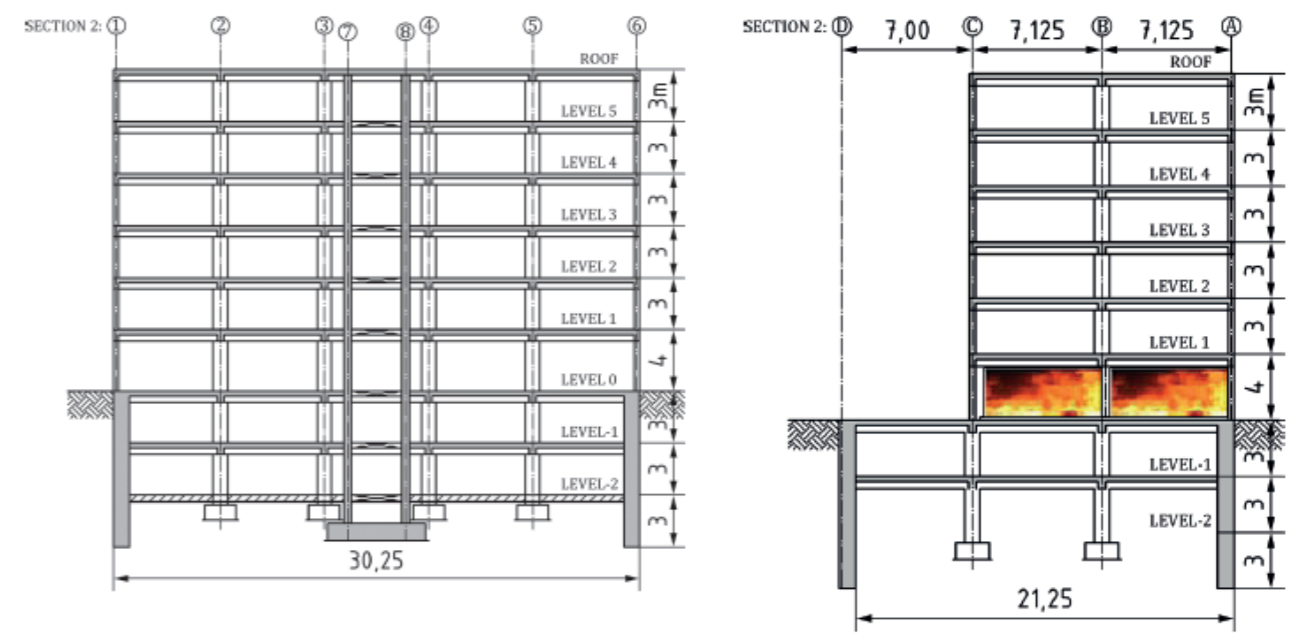
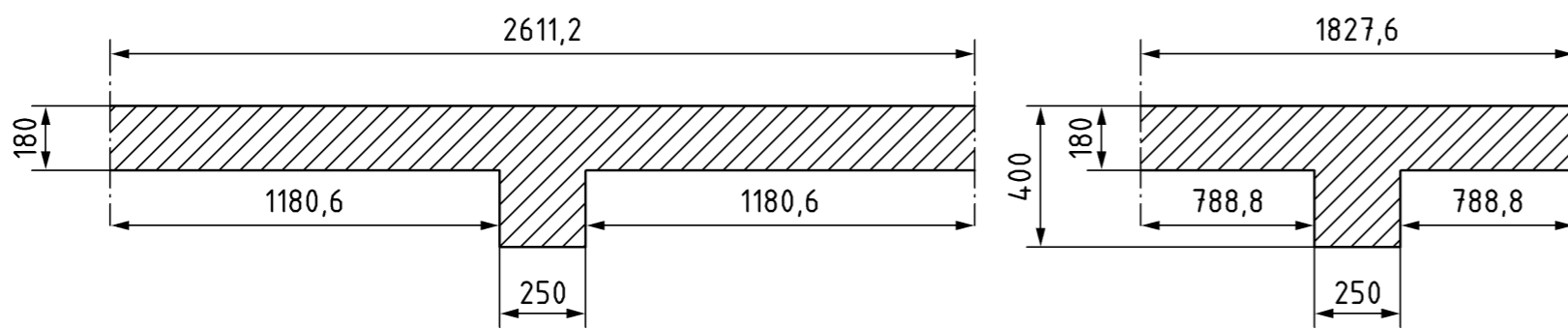
### Step 1: Scope of the project (for fire safety of structures)

#### Eurocode reference building

Biasoli et al. (2014). ec.europa.eu



	Load	Value of load
Dead load	Self-weight	25 kN/m <sup>3</sup>
	Finishing	1,5 kN/m <sup>2</sup>
Live load	Office	4 kN/m <sup>2</sup>





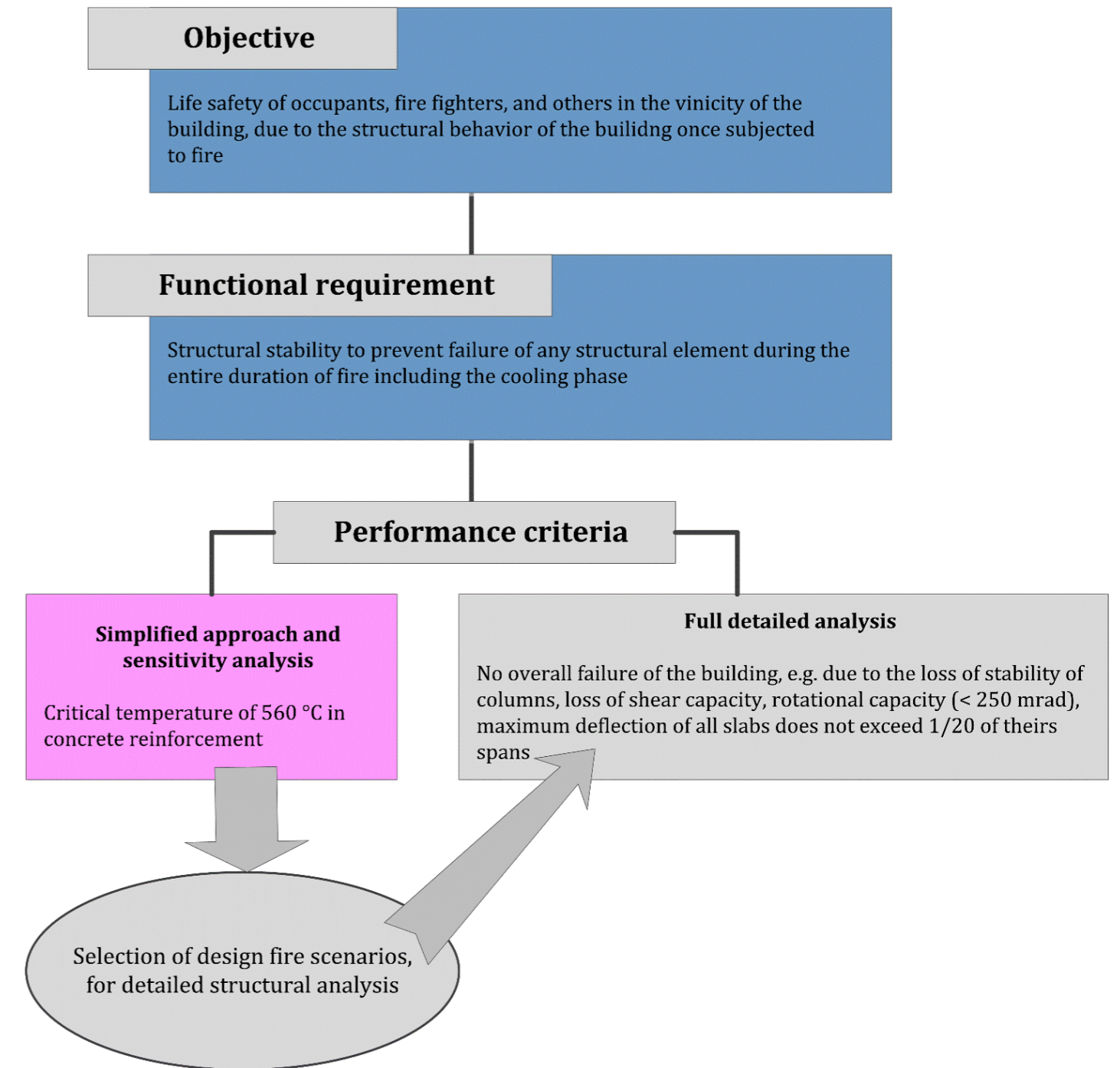
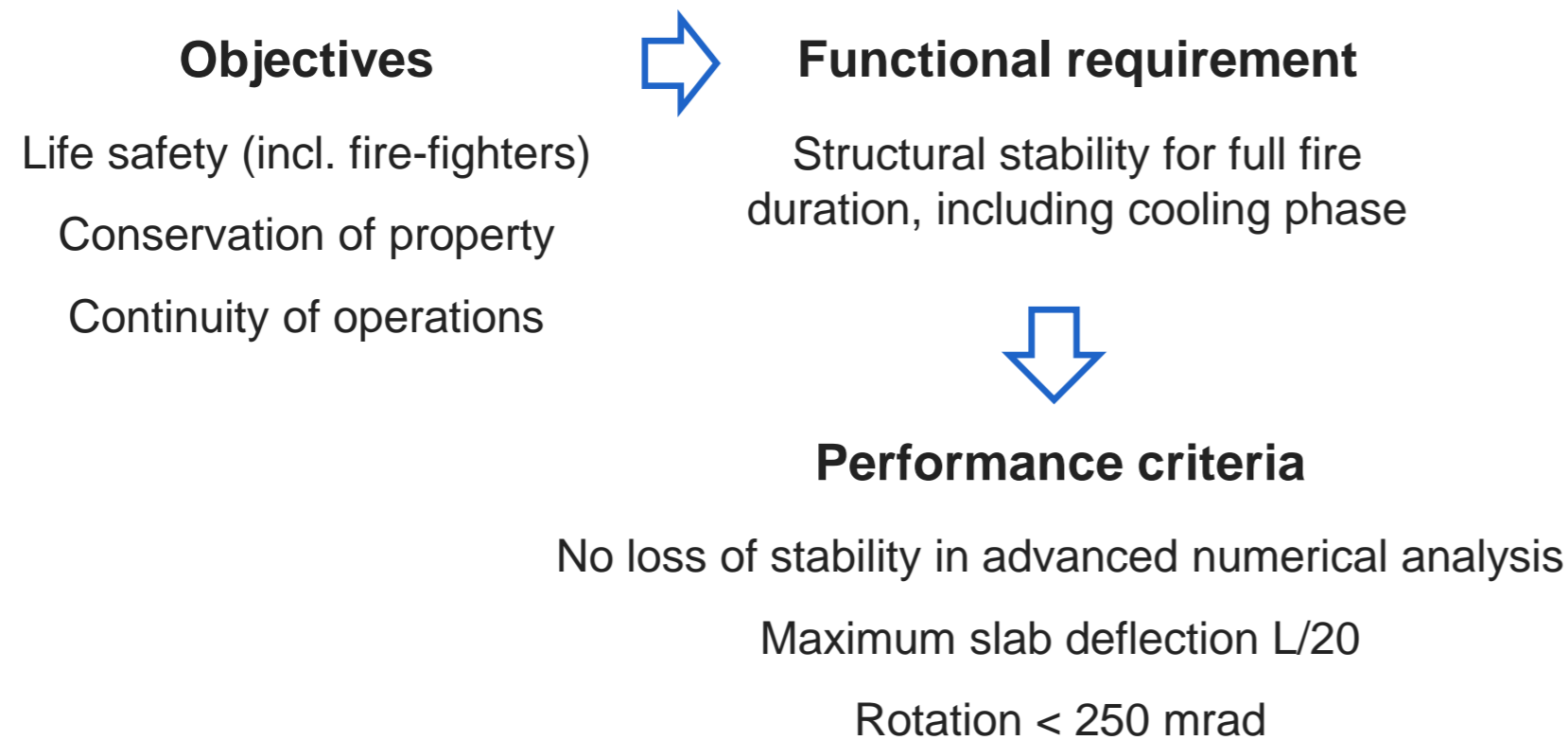
# STRUCTURAL FIRE ENGINEERING FRAMEWORK

## Structural fire engineering framework

### ISO 24679-1:2017. Fire safety engineering – Performance of structures in fire

ISO TR 24679-6:2017. Fire safety engineering – Performance of structures in fire – Part 6:  
Example of an eight storey office concrete building. *International Organization for Standardization.*

### Step 2: Identifying objectives, functional requirements and performance criteria





# STRUCTURAL FIRE ENGINEERING FRAMEWORK

## Structural fire engineering framework

### ISO 24679-1:2017. Fire safety engineering – Performance of structures in fire

ISO TR 24679-6:2017. Fire safety engineering – Performance of structures in fire – Part 6: Example of an eight storey office concrete building. *International Organization for Standardization.*



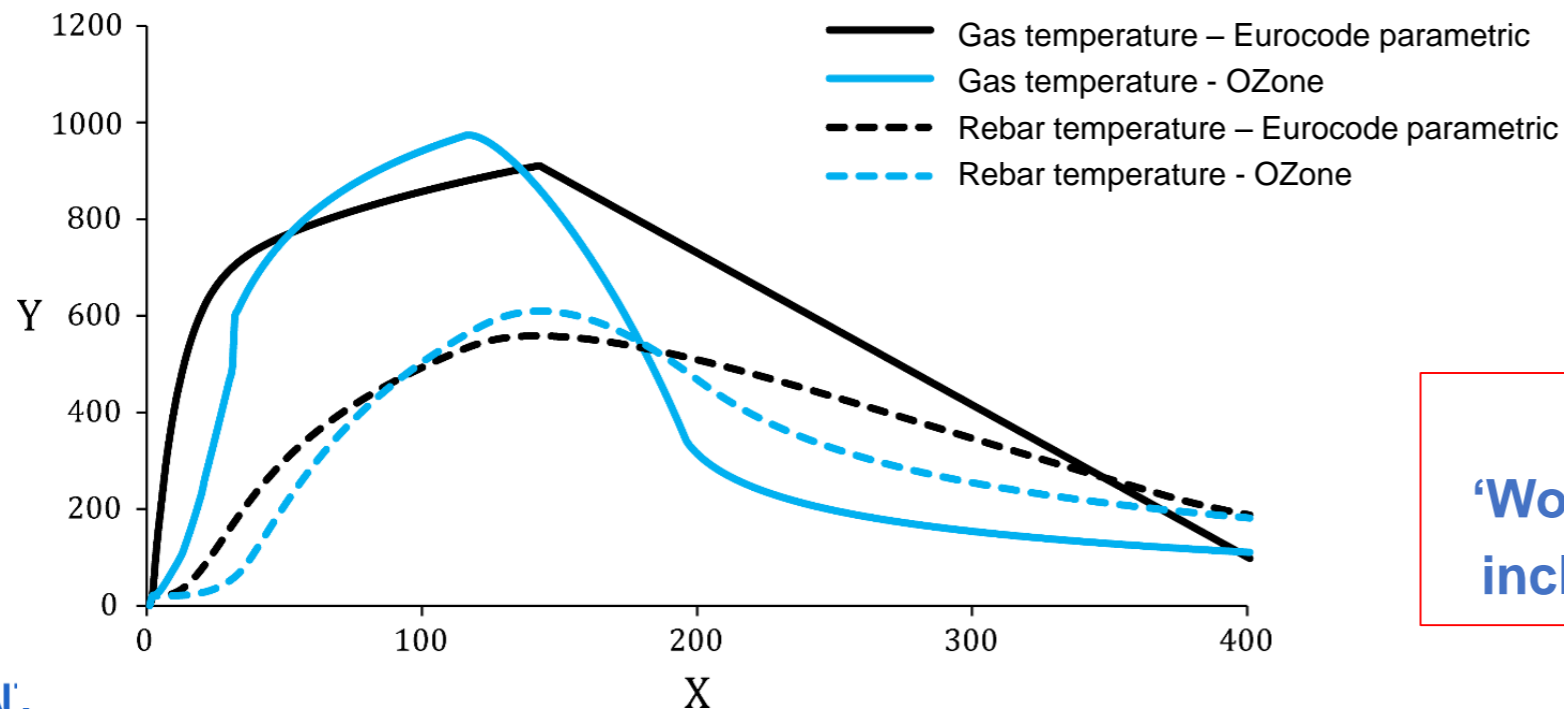
### Step 3: Trial design plan

Eurocode reference building, with floor compartmentation

### Step 4: Design fire scenarios and design fires

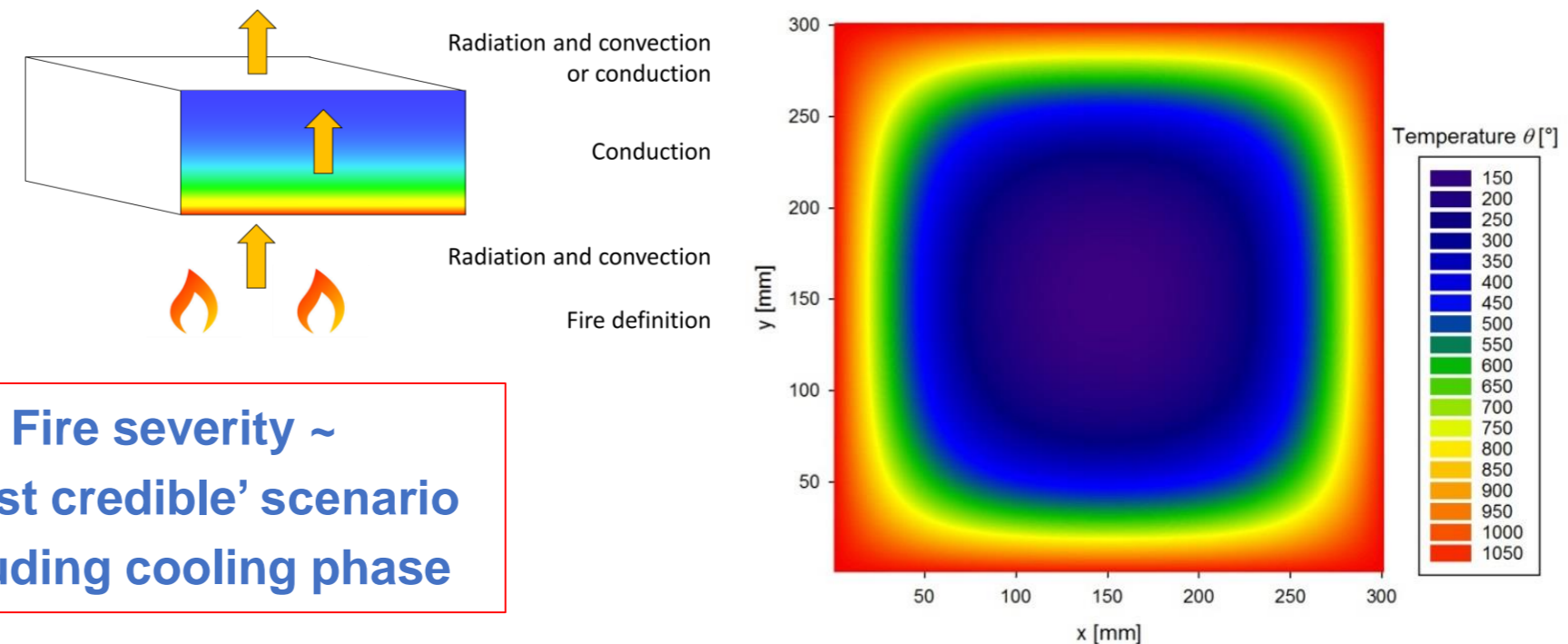
Eurocode parametric fire, design fire load 912 MJ/m<sup>2</sup>; opening factor 0,02 m<sup>1/2</sup>

Heidari et al. (2018). *Fire Technology*, in press.



### Step 5: Thermal response of the structure

SAFIR Franssen, J. M., & Gernay, T. (2017). Modeling structures in fire with SAFIR®: theoretical background and capabilities. *Journal of Structural Fire Engineering*, 8(3), 300-323.



Fire severity ~  
‘Worst credible’ scenario  
including cooling phase

# STRUCTURAL FIRE ENGINEERING FRAMEWORK

## Structural fire engineering framework

### ISO 24679-1:2017. Fire safety engineering – Performance of structures in fire

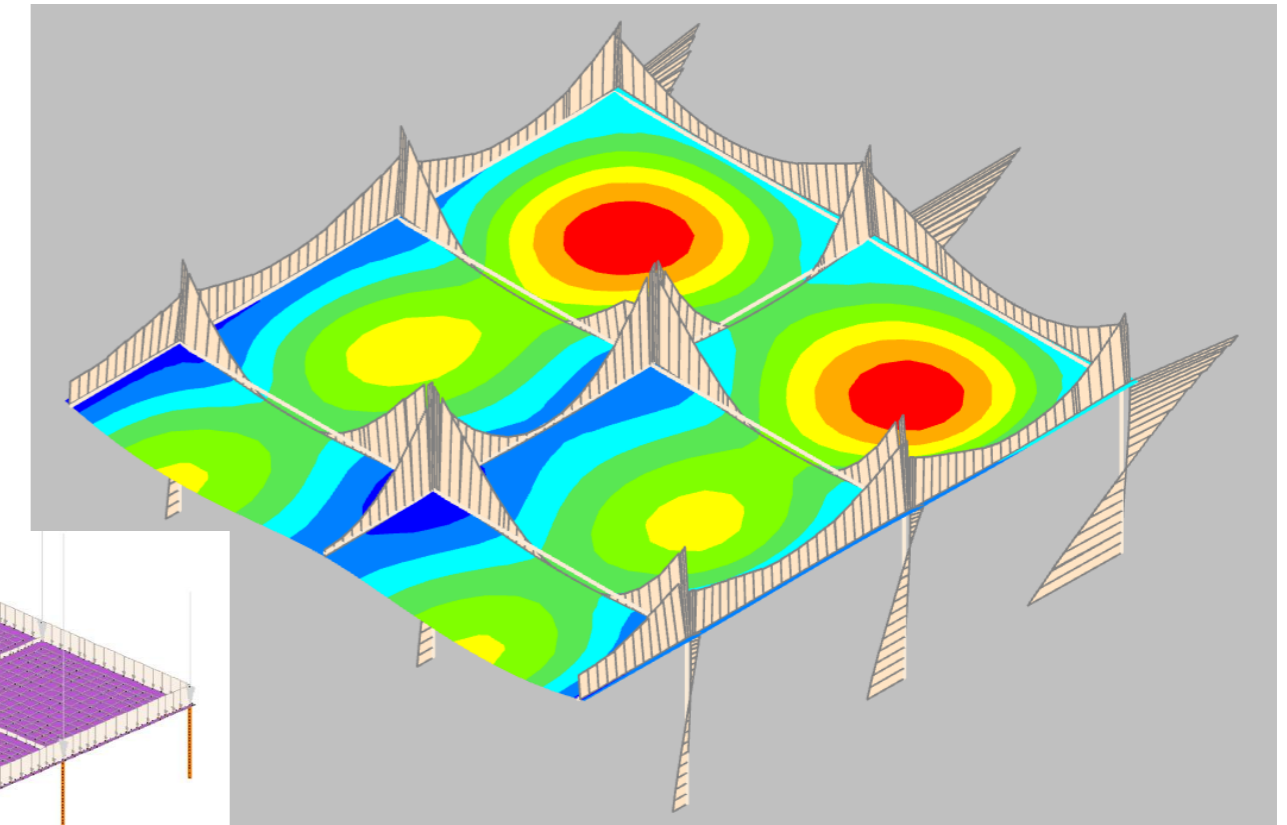
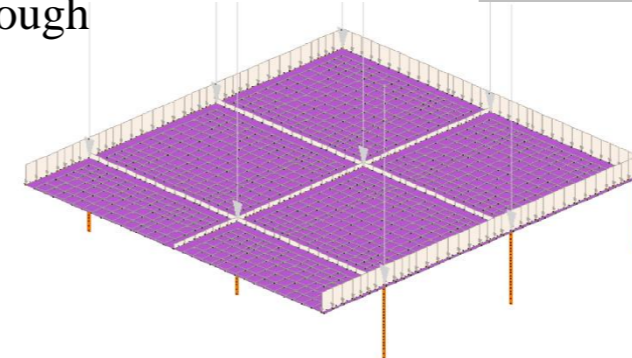
ISO TR 24679-6:2017. Fire safety engineering – Performance of structures in fire – Part 6:  
Example of an eight storey office concrete building. *International Organization for Standardization.*

Sauca, et al. (2016). Analysis of a concrete building exposed to natural fire. *Applications of Structural Fire Engineering.*

### Step 6: Mechanical response of the structure

SAFIR Franssen, J. M., & Gernay, T. (2017). Modeling structures in fire with SAFIR®: theoretical background and capabilities. *Journal of Structural Fire Engineering*, 8(3), 300-323.

- (i) plane sections remain plane (Bernoulli hypothesis);
- (ii) effects of non-uniform temperature distribution in the section considered through a fiber model;
- (iii) shear energy of the plane sections ignored;
- (iv) uniaxial constitutive models;
- (v) large displacements are considered but strains are assumed small.



### Step 7: Assessment against the fire safety objectives

Structural stability up to full burnout confirmed  
Maximum deflections do not exceed  $L/20$   
Rotation does not exceed 250 mrad



**‘Burnout resistance’**  
confirmed for  
**‘worst credible scenario’**

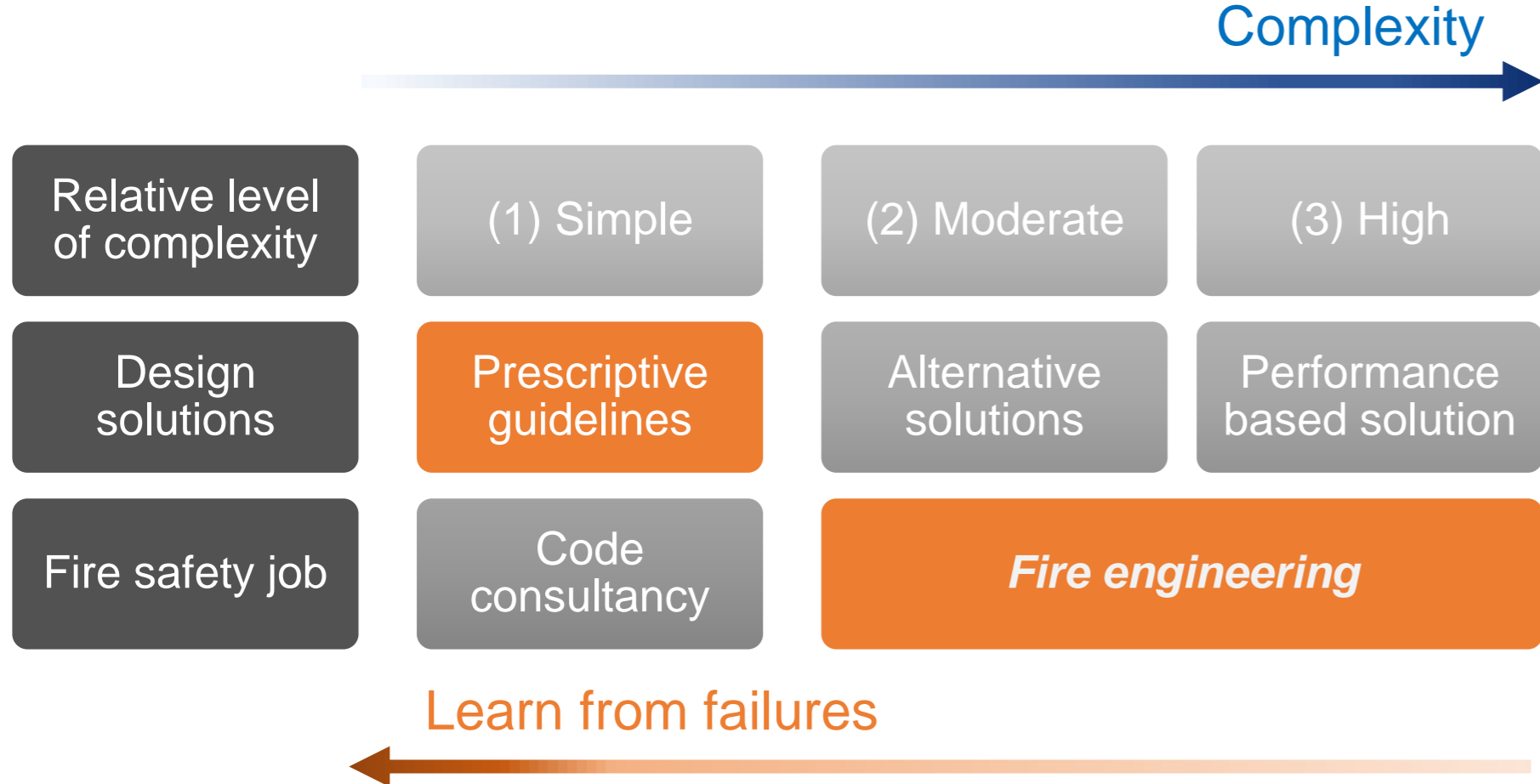


**Life safety** (fire fighters)  
Other floors unaffected  
(strengthening required)  
**Conservation of property**  
**Continuity of operations**

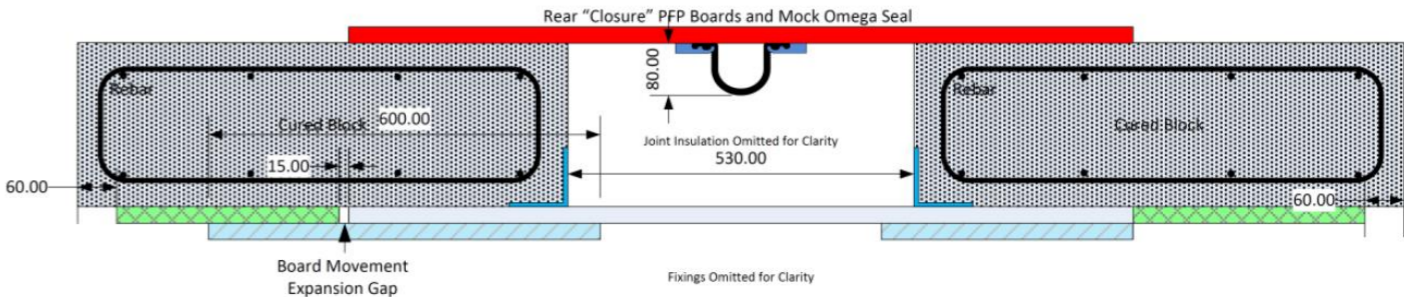
**More info vs prescriptive**



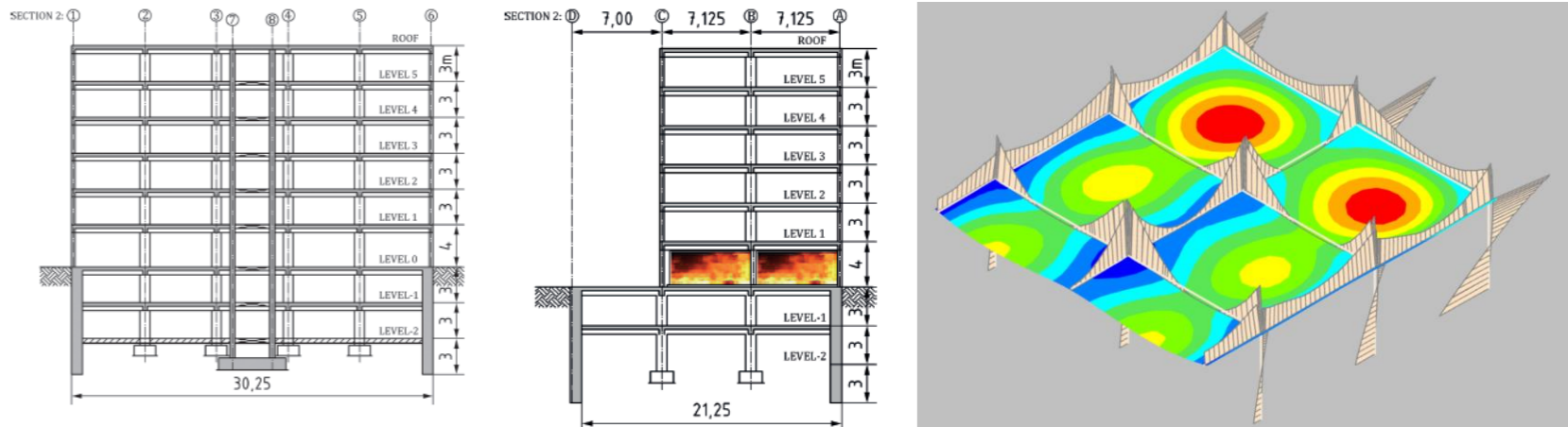
# STRUCTURAL FIRE ENGINEERING FRAMEWORK



## Design beyond prescriptive guidance



## Clear target performance (vs prescriptive)



Institution of Fire Engineers

**Fire engineering** is the application of scientific and engineering principles, based on an understanding of the phenomena to protect people, property and the environment from fire



# Structural fire engineering: risk and opportunities





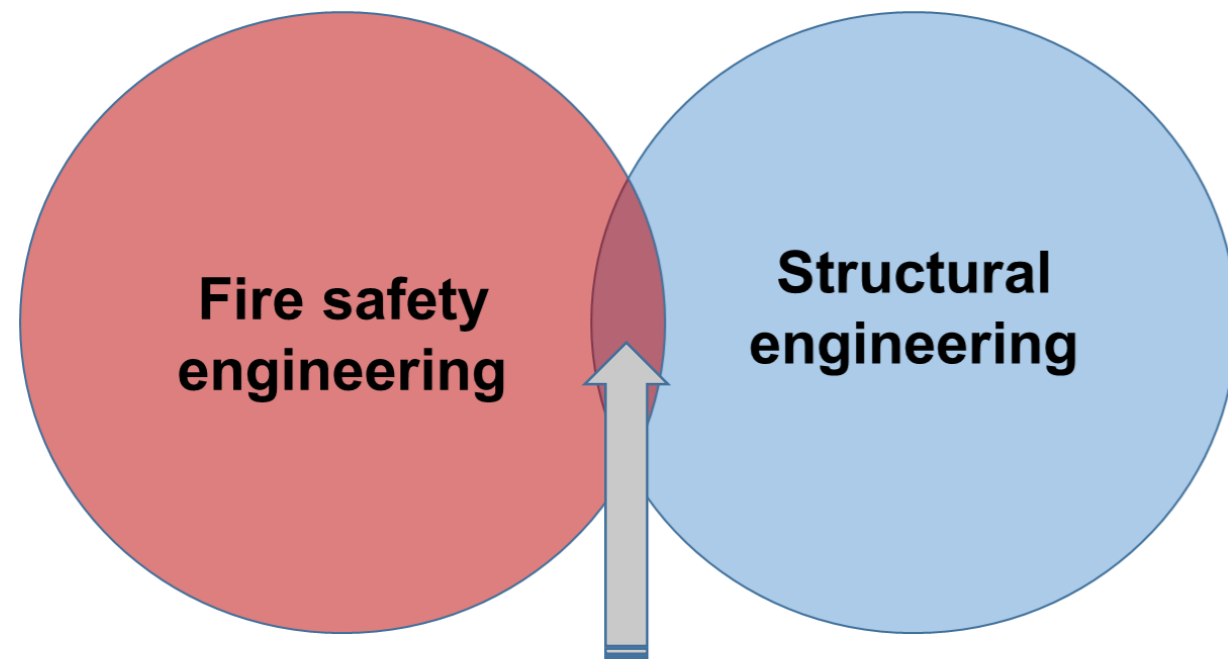
# RISK OF INAPPROPRIATE USE

To assess relative to the fire safety goals / objectives



*Application scientific and engineering principles, understanding of the phenomena to protect people, property and the environment*

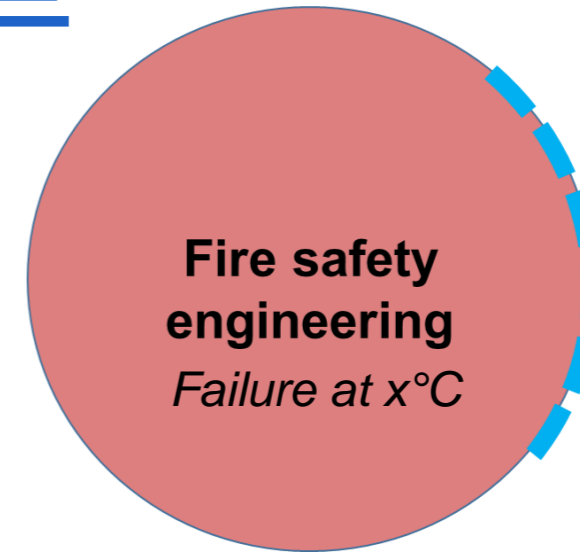
Prof. G. Rein, Imperial College



**Structural design for fire safety**

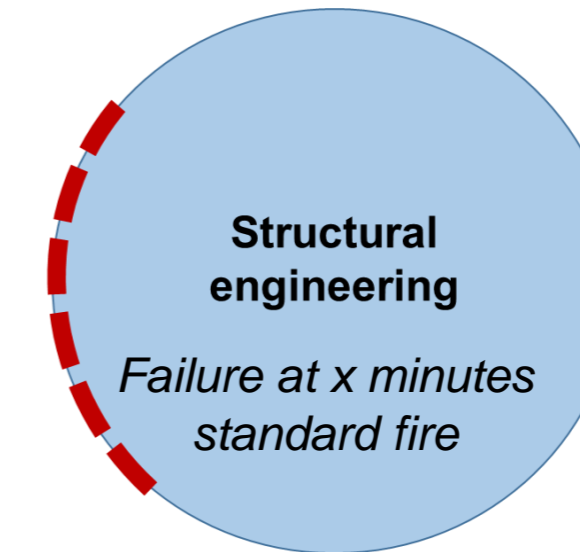
**Lame substitution of the 1<sup>st</sup> kind**

Structural engineering replaced by pseudo-science



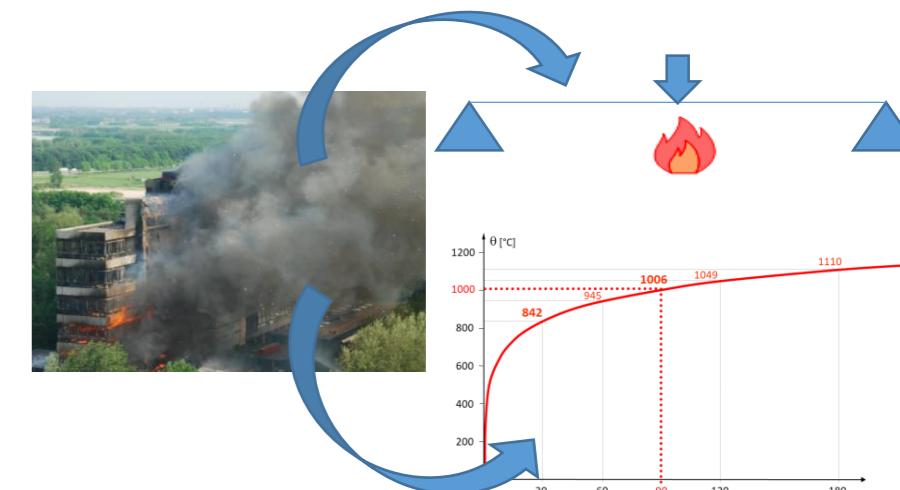
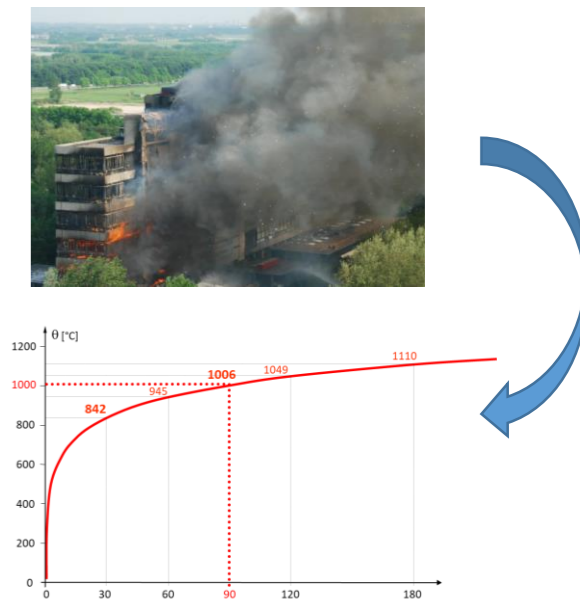
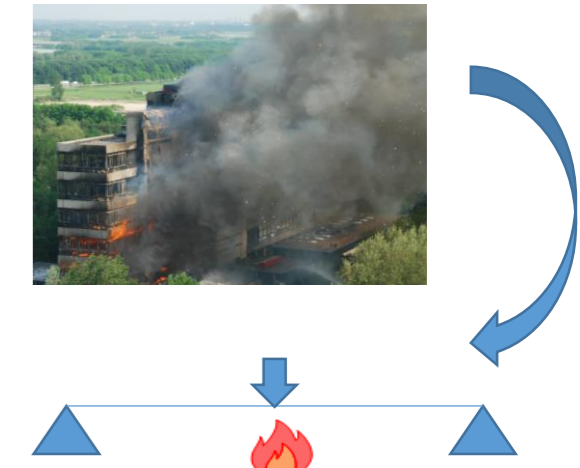
**Lame substitution of the 2<sup>nd</sup> kind**

Fire engineering replaced by pseudo-science



**Lame substitution of the 3<sup>rd</sup> kind**

Both structural and fire engineering replaced by pseudo-science



Hopkin, D. (2018). Guest lecture Ghent University.

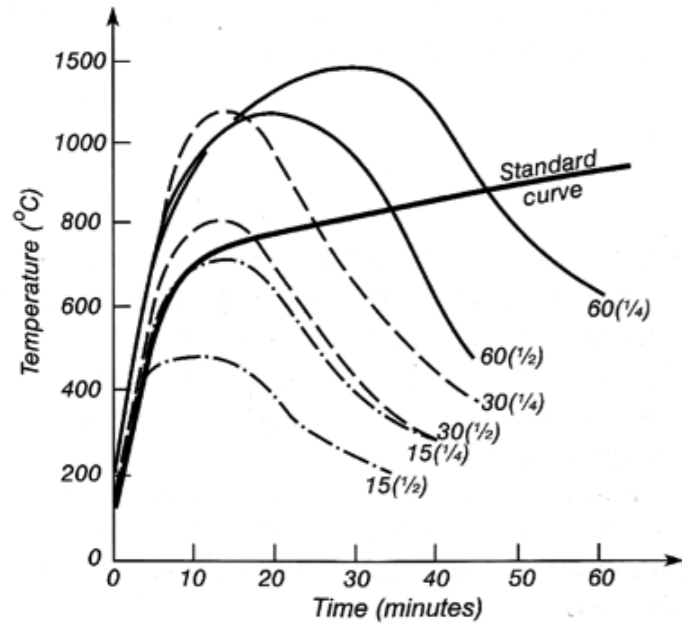


# OPPORTUNITY – CLARIFYING FIRE SEVERITY (1)

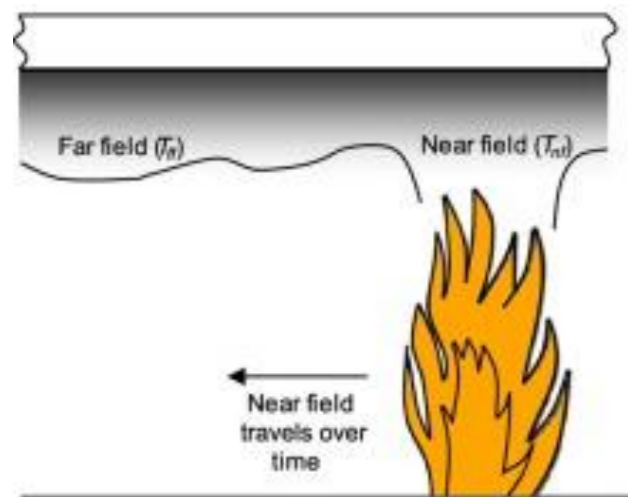
Compartment fires don't resemble the ISO curve...

The Eurocode parametric fire is particularly popular

Simplified and advanced fire models provide a better description



Buchanan, A. H., & Abu, A. K. (2017). *Structural design for fire safety*. John Wiley & Sons.



Stern-Gottfried & Rein. (2012). *Fire Safety Journal*, 54, 96-112.

**\*) Nominal time-temperature curve**

Standard fire curve, external fire curve & hydrocarbon curve

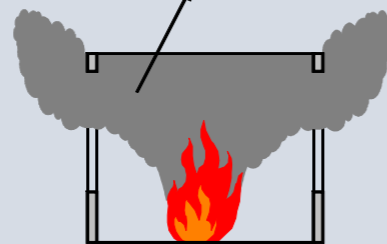
No data required

**\*) Simplified fire models**

**Localized fire**

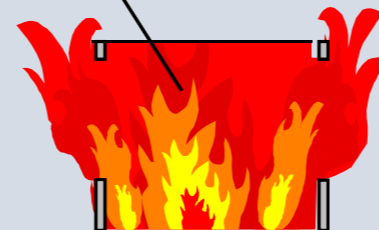
- HESKESTADT
- HASEMI

$$\theta(x, y, z, t)$$



**Full compartment fire**

- Parametric fire
- $\theta(t)$  uniform in the compartment



**\*) Advanced fire models**

- Two-Zone model
- One-Zone model
- Combination Two-Zone and One-Zone
- CFD

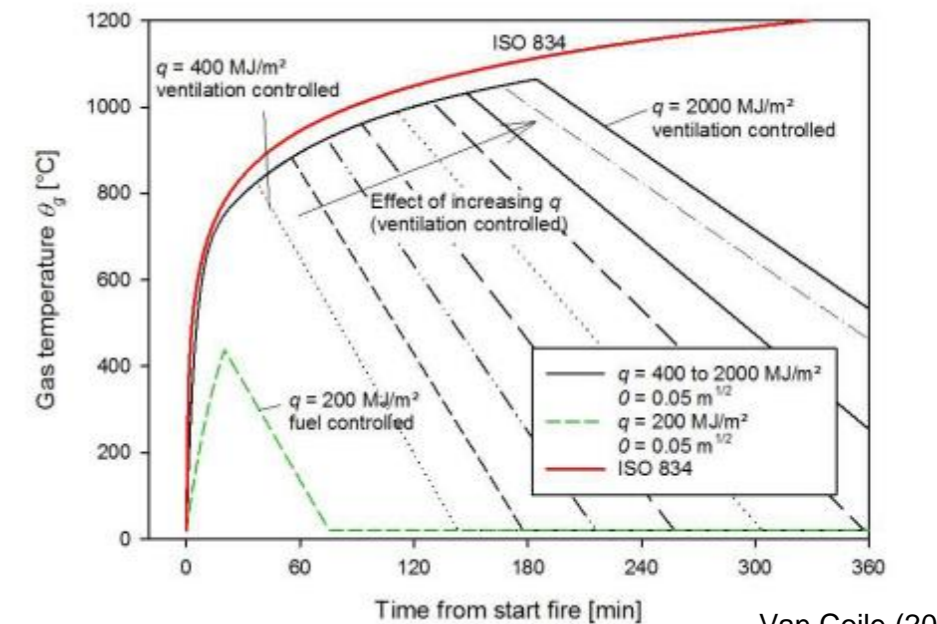
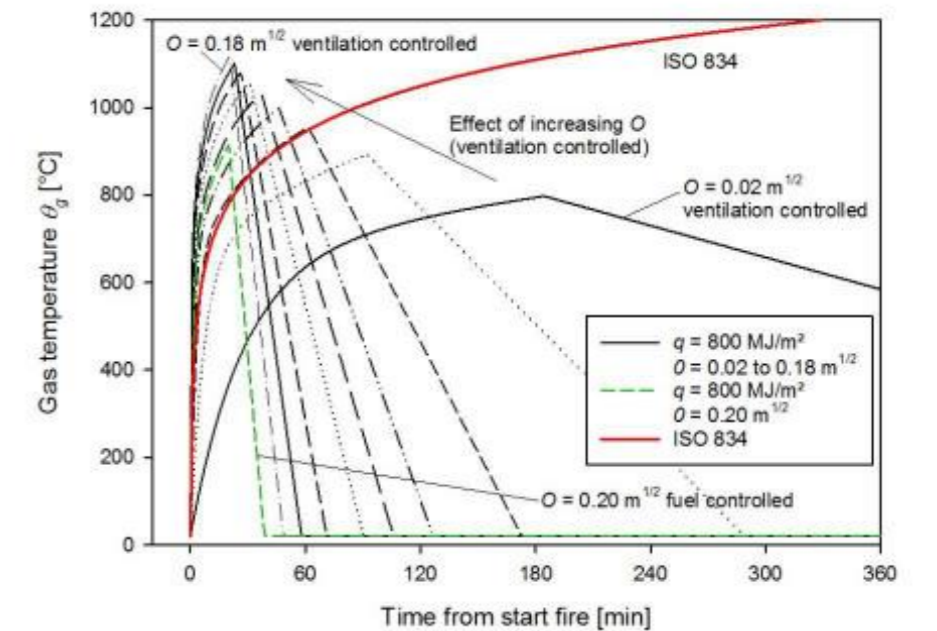
- Rate of heat release
- Fire surface
- Fire load density
- Boundary properties
- Area of openings
- Ceiling height

+  
Exact geometry

DIFISEK (2009); Gernay, T. (2018). Lecture notes Structural Fire Engineering.

Ozone; SAFIR (trial version available)  
<https://www.uee.uliege.be>

- Fire load  $q_F$  [MJ/m<sup>2</sup>]
- Ventilation condition,  $O$  [m<sup>1/2</sup>]



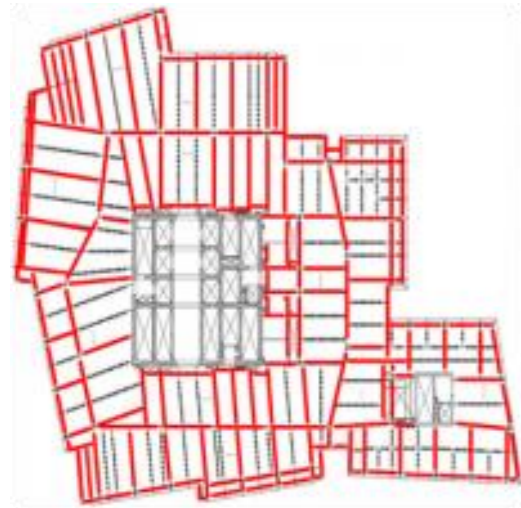
Van Coile (2015).



# OPPORTUNITY – CLARIFYING FIRE SEVERITY (2)

...but the ISO curve isn't leaving (soon)

- Engineers use it to specify requirements
- Manufacturers to specify their products
- Legislators to set requirements



WSP. The Shard.



Approved Document B (UK)

Table 3bm. CAFCO® 300 thicknesses for I section beams and columns. Limiting temperature 620°C

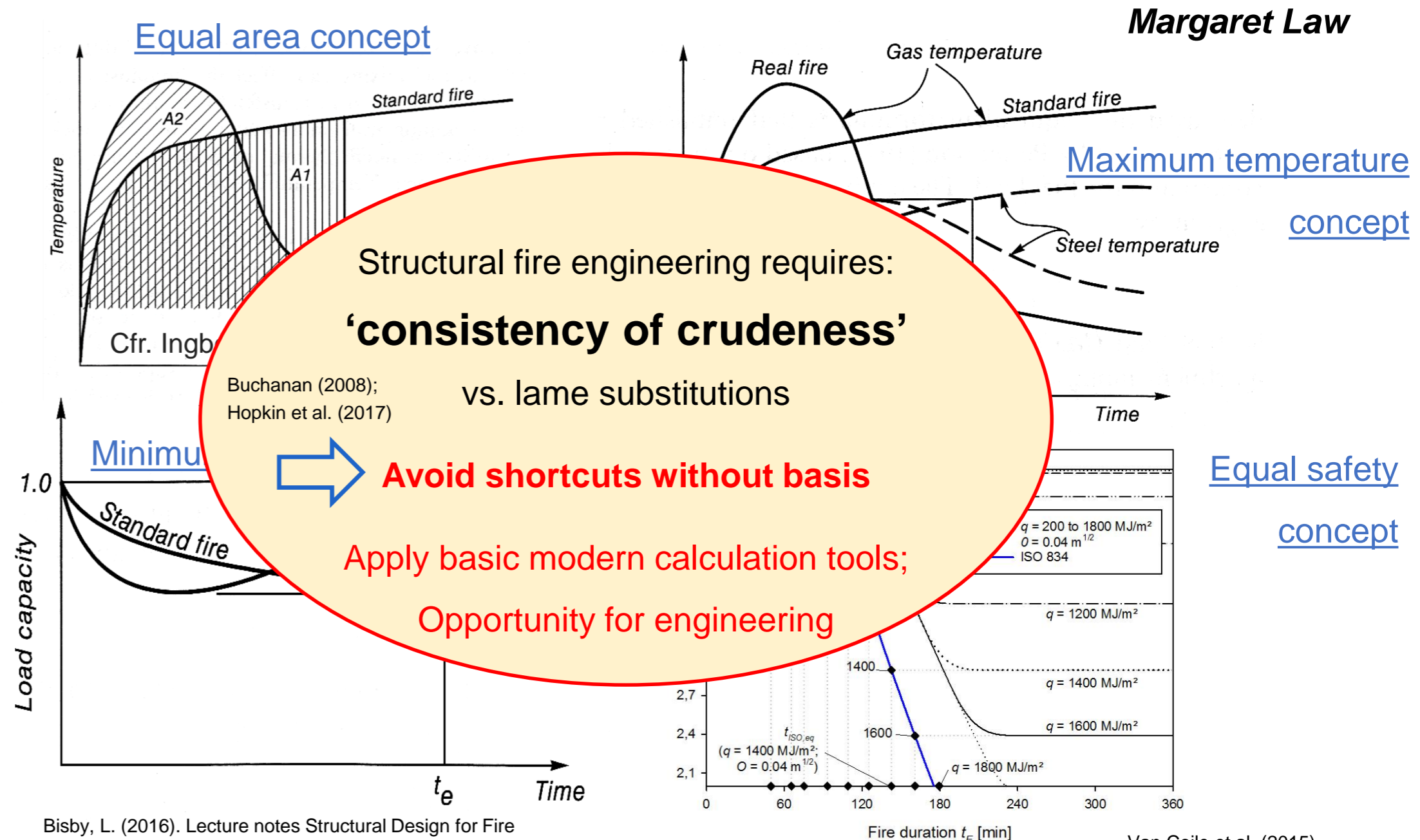
A/V	CAFCO® 300 thickness (mm) for fire resistance of:					
	30 (mins)	60 (mins)	90 (mins)	120 (mins)	180 (mins)	240 (mins)
30	12	12	12	12	16	20
40	12	12	12	13	19	25
50	12	12	12	15	22	28
60	12	12	13	16	24	31

PROMAT. The passive fire protection handbook.

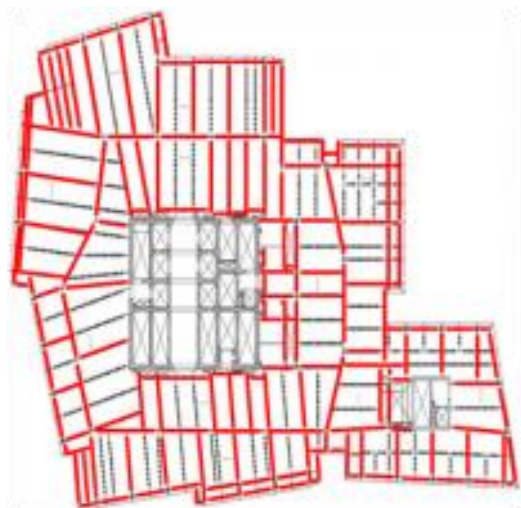
## Equivalent standard fire duration

**Caution advised:** Law, M. (1997). A review of formulae for T-equivalent. *Fire Safety Science*, 5, 985-996.

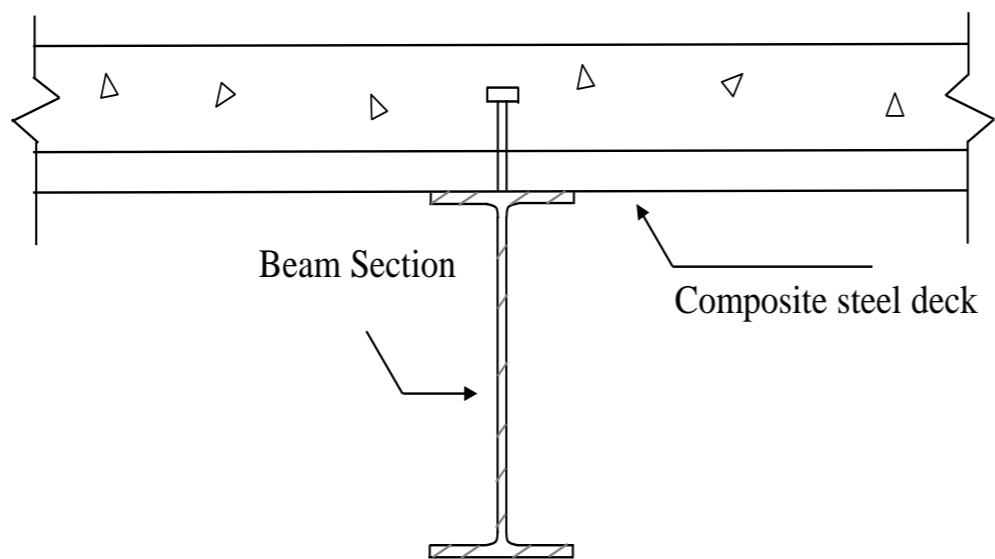
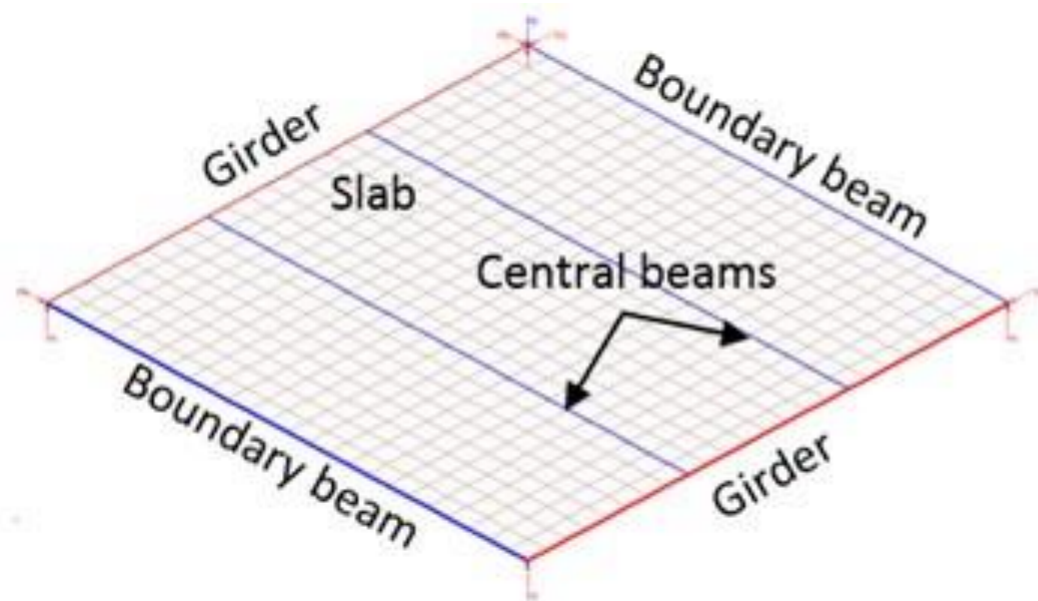
*“t-equivalent is not a useful parameter for design purposes”*



# OPPORTUNITY – COST MINIMIZATION

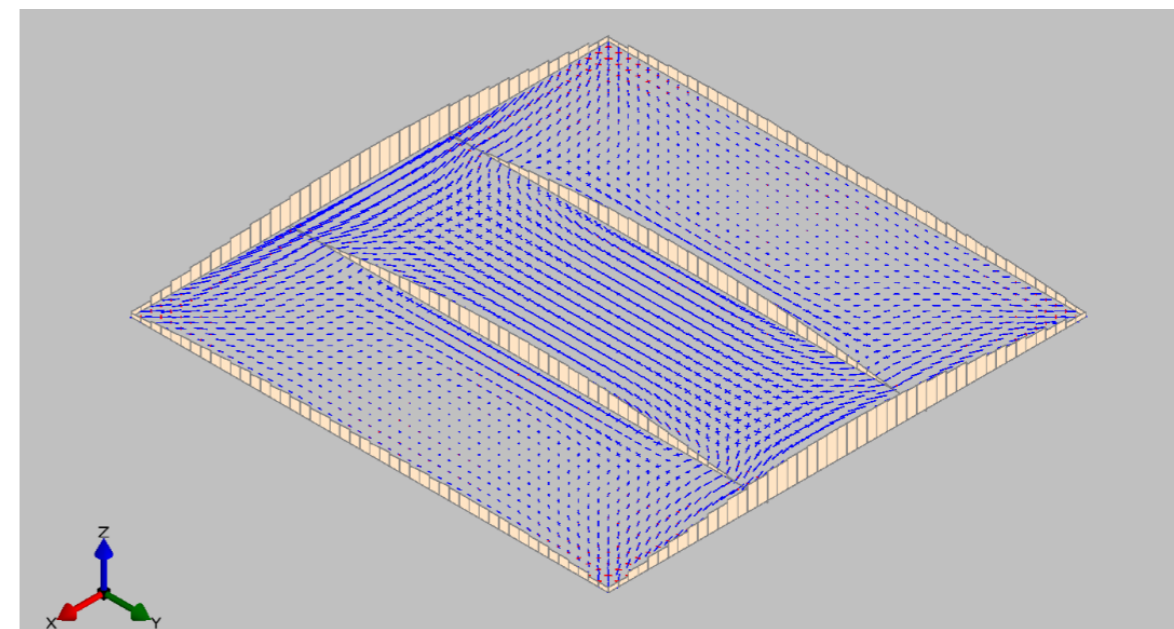


WSP. The Shard.

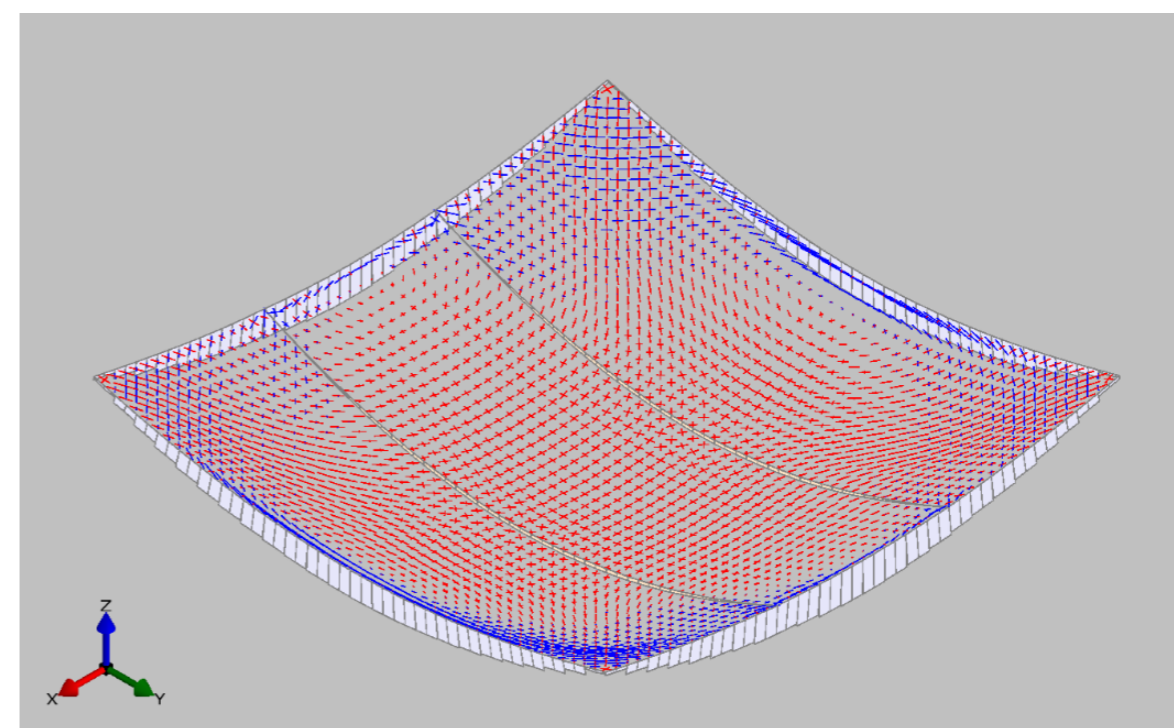


Elhami Khorasani, et al. (2017). Comparative fire analysis of steel-concrete composite buildings designed following performance-based and US prescriptive approaches. *Proceedings of ASFE 2017*, 07-08/09, Manchester, UK, pp. 131-140.

Normal design situation

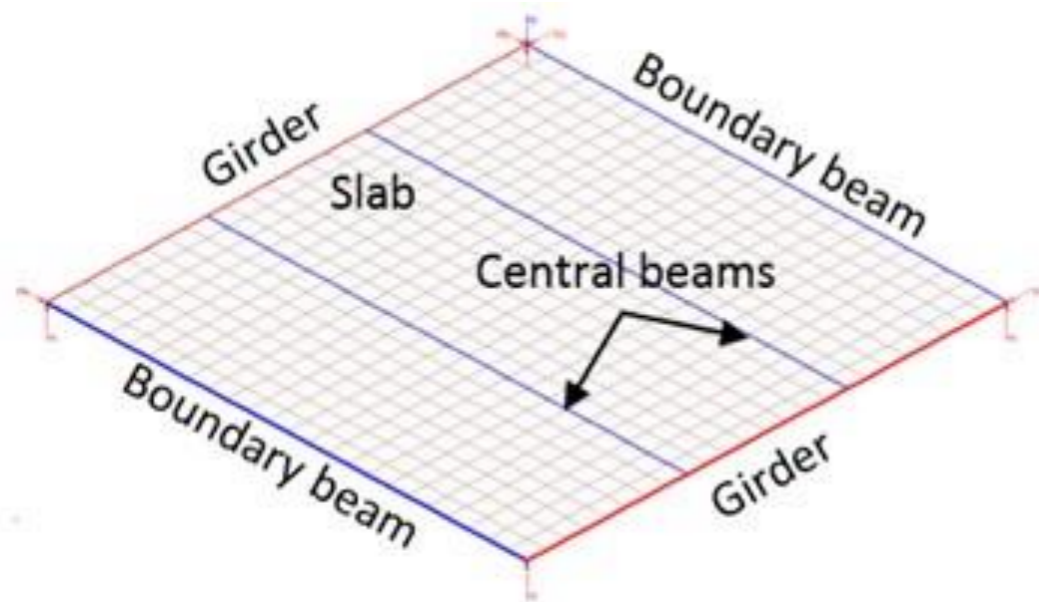
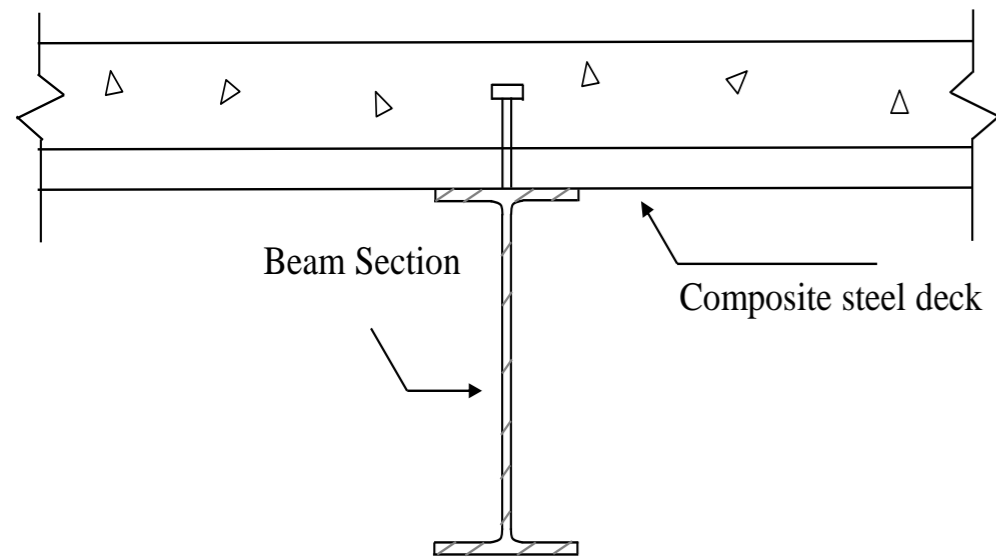


Fire design situation





# OPPORTUNITY – COST MINIMIZATION



Elhami Khorasani, et al. (2017). *Proceedings of ASFE 2017*, 07-08/09, Manchester, UK, pp. 131-140.

- Stability (and compartmentation) maintained including cooling phase;
- Large permanent deformations

# OPPORTUNITY – COST OPTIMIZATION (1)

## Lifetime cost:

$$Y = C + A + D_M + D_L + D_R$$

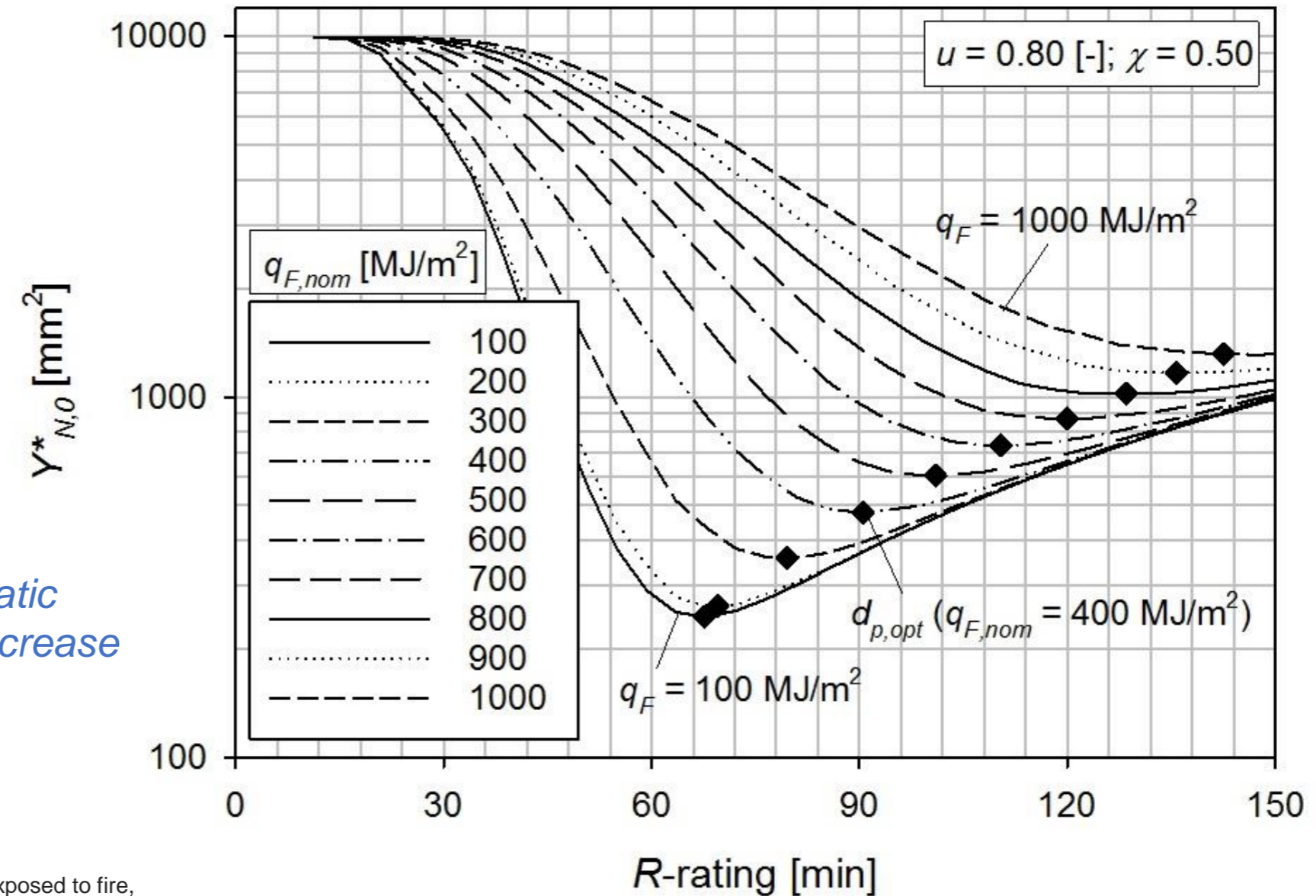
*Travelling fire / parametric fire  
if room conditions*

Symbol	Description
$Y$	Lifetime cost
$C$	Total building construction and maintenance cost
$A$	Obsolescence cost
$D_M$	Fire-induced material damages
$D_L$	Fire-induced loss to human life and limb
$D_R$	Reconstruction cost after fire-induced failure

## Cost of fire protection

Fire rating	Cost [GBP/m <sup>2</sup> ]	Indicative thickness $d_p$ [mm]*	Eq. Cost [GBP/m <sup>2</sup> ]
30 min	5-8	5	6.0
60 min	8-12	12	10.8
90 min	18-20	19	19.4
120 min	30-35	25	30.0

*Quadratic  
cost increase*



Van Coile, R., & Hopkin, D. (2018). Target safety levels for insulated steel beams exposed to fire, based on Lifetime Cost Optimisation. *Proceedings of IALCCE 2018*. Taylor & Francis Group.



# OPPORTUNITY – COST OPTIMIZATION (2)

## London office building

Description & reference	Value	Units
Number of occupied storeys	5	[-]
Building height	< 30	[m]
Ignition rate per floor (BSI, 2003)	$6 \cdot 10^{-3}$	[y <sup>-1</sup> ]
Probability of ignition resulting in a fully developed fire (EC, 2002)	0.9	[-]
Nominal fire load density (CEN, 2002b)	400	[MJ/m <sup>2</sup> ]
Building cost (Turner & Townsend, 2016)	2,700	[£/m <sup>2</sup> ]
Structural grid	7.5x7.5	[m x m]
Ambient utilisation (u)	0.55	[-]
Load ration ( $\chi$ )	0.42	[-]
Fire utilisation ( $u_{fi}$ )	0.31	[-]
Relative total material failure cost ( $\xi_M$ ), (Kanda and Shah, 1997)	7.0	[-]

$\xi_M = 1.4$  per floor; all floors affected by failure

$\xi_L = 0 - 9.6$  (average of 0 – 10 casualties)

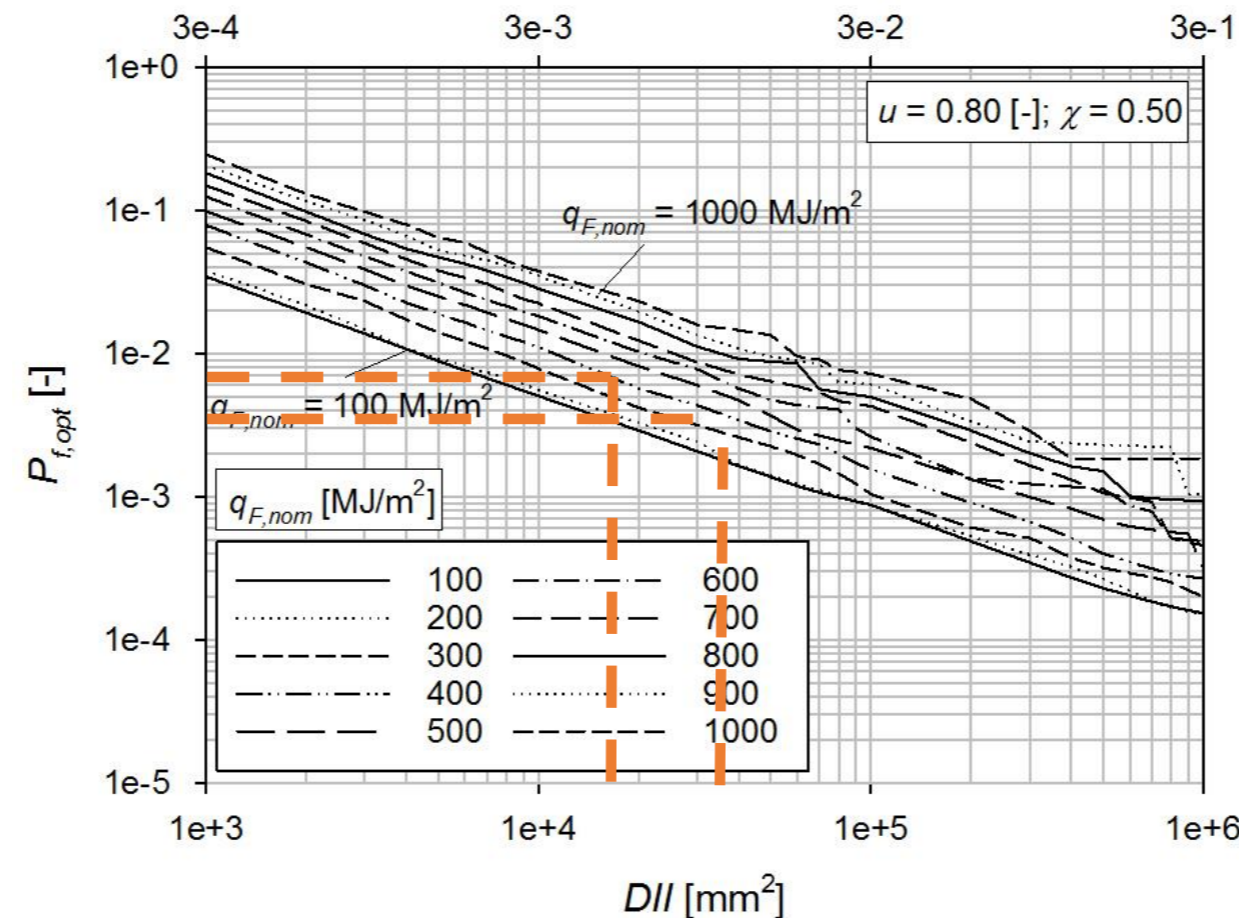
$\gamma = \omega = 0.02$        $a_{2,N} = 7.5 \cdot 10^{-6} \text{ mm}^{-2}$

➔  $DII = 1.4 \cdot 10^4 \text{ mm}^2 - 3.3 \cdot 10^4 \text{ mm}^2$

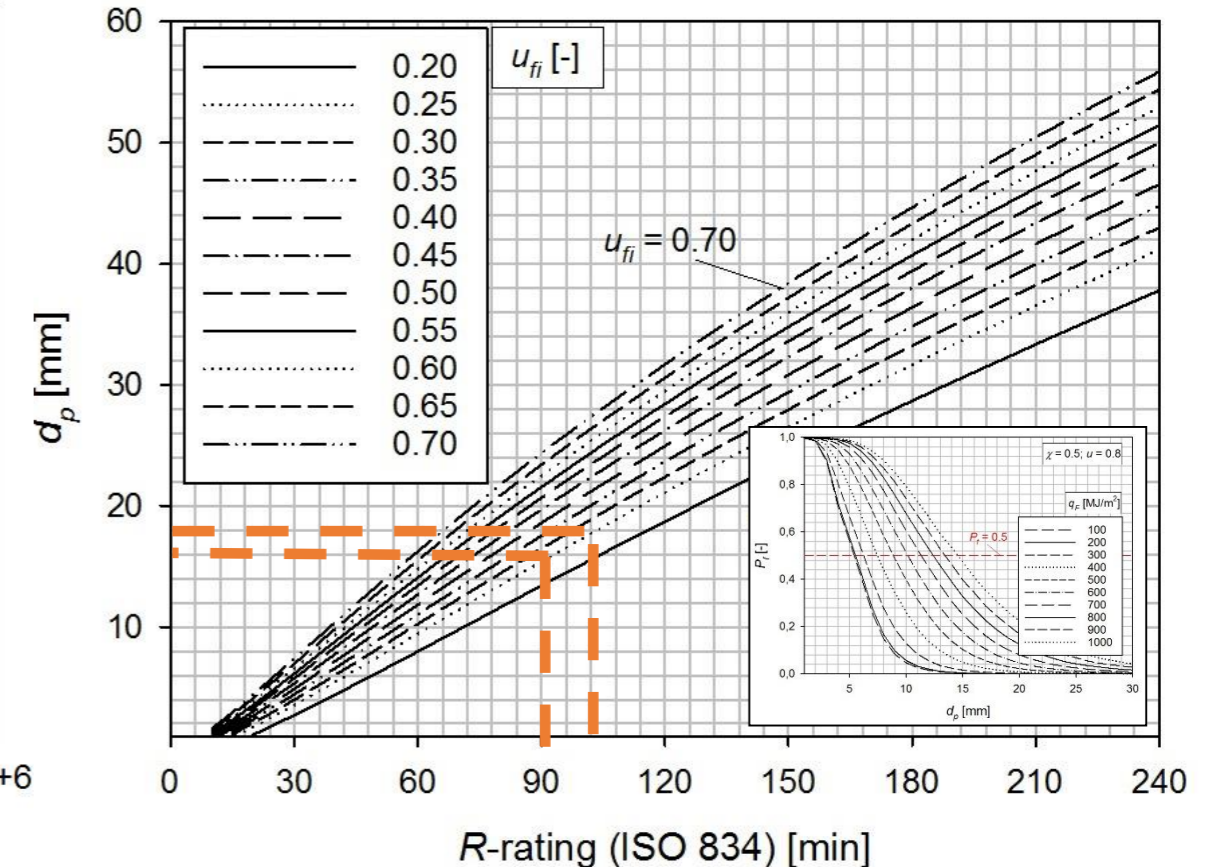
↳ ratio of structural fire damage to investment cost intumescent paint per [mm]<sup>2</sup>

## Optimum failure probability i.f.o. DII

$$\lambda_{fi} \cdot (\xi_M + \xi_L) [1/\text{year}], \text{ when } a_{2,N} \cdot (\gamma + \omega) = 3 \cdot 10^{-7} \text{ mm}^{-2}$$



## $P_f$ i.f.o. protection thickness Relationship thickness – R-rating



➔ **Optimum fire-rating  $R_{opt} = 90 - 100$  min**

(slightly above UK prescriptive guidance; no practical influence  $\xi_L$ )

- Optimized R-specifications for high level projects
- Benchmarking prescriptive guidance



GHENT  
UNIVERSITY

Van Coile, R., & Hopkin, D. (2018). Target safety levels for insulated steel beams exposed to fire, based on Lifetime Cost Optimisation. *Proceedings of IALCCE 2018*. Taylor & Francis Group.

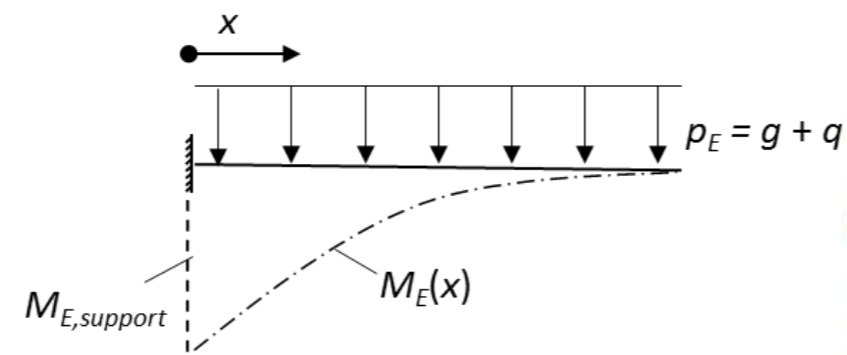


# OPPORTUNITY – IMPROVED PERFORMANCE

## Exclusive apartments London



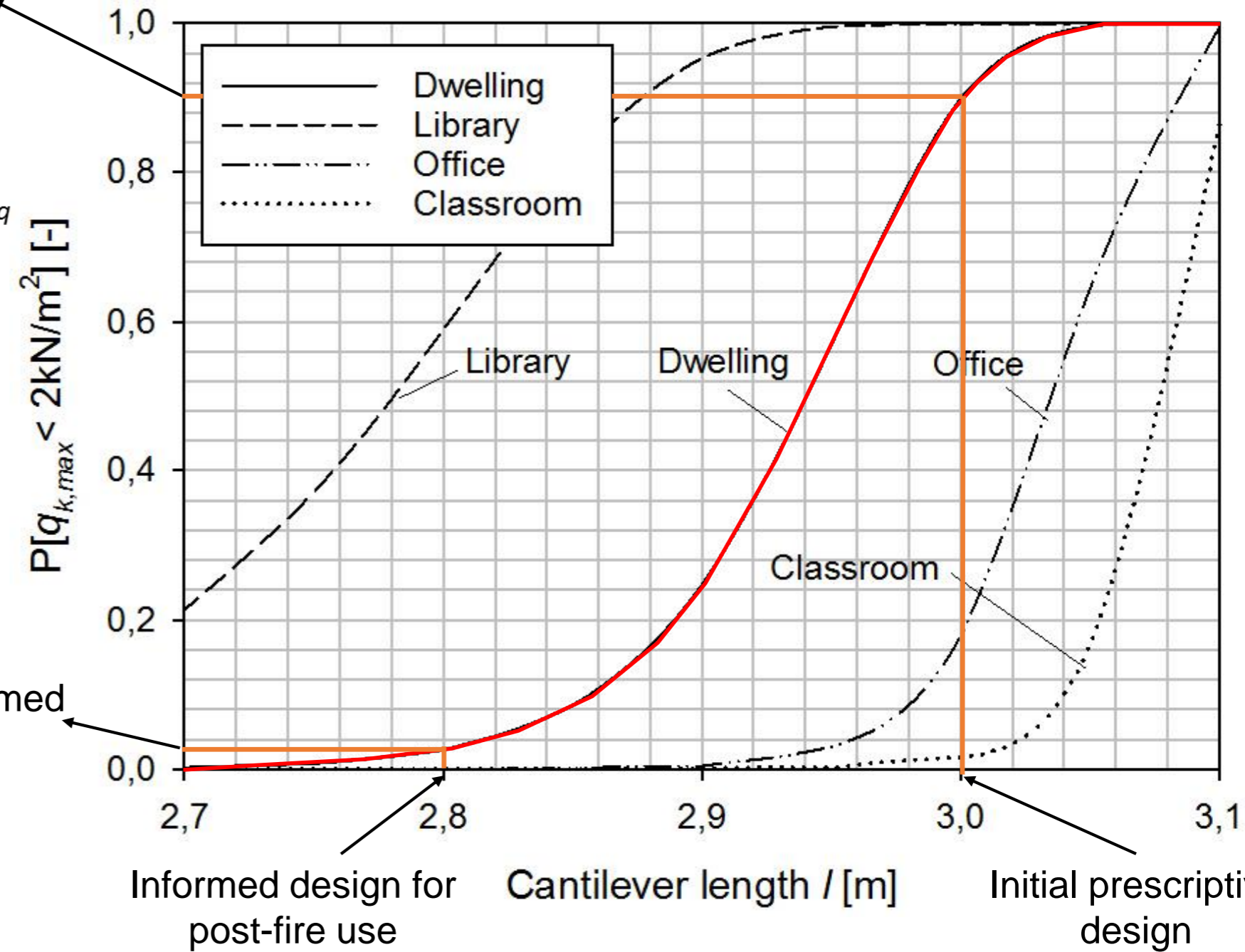
Cantilever slab



Length  $l$  of the cantilever as decision variable

Initial probability of not achieving requirement

Fragility curves for  $q_{k,req} = 2\text{kN/m}^2$



## Resilience requirement:

Fire in compartment below may not affect usability (safety) of compartment above

➔  $q_{k,req} = 2\text{ kN/m}^2$  post-fire



*In conclusion:*

Fire engineering  
*application of scientific and engineering principles,  
based on an understanding of the phenomena  
to protect people, property and the environment from fire*



[www.linkedin.com/in/rubenvancoile/](https://www.linkedin.com/in/rubenvancoile/)  
<https://biblio.ugent.be/person/002005283121>

*Thank you*